



HI-TECH INSTITUTE OF TECHNOLOGY, KHURDA, BHUBANESWAR, ODISHA

**CLASS NOTES ON**

**ELECTRICAL ELECTRONICS MEASUREMENTS**

**FOR**

**4TH SEMESTER OF**

**ELECTRICAL ENGINEERING (B.TECH PROGRAMME)**



## PEE3I104 ELECTRICAL AND ELECTRONICS MEASUREMENT

### Module- I

[10 Hours]

#### University Portion (80%): (8 Hours)

Measurement and Error: (2Hrs) Definition, Accuracy and Precision, Significant Figures, Types of Errors. Text book-2-Ch-[1.1 to 1.4]

Standards of Measurement: (1 Hrs) Classification of Standards, Electrical Standards, IEEE Standards. Text Book-2- Ch-[3.1,3.4,3.6]

Types of measuring instrument: (5 Hrs) Ammeter and Voltmeter: Derivation for Deflecting Torque of; PMMC, MI (attraction and repulsion types), Electro Dynamometer and Induction type Ammeters and Voltmeters. Energy meters and wattmeter.: Construction, Theory and Principle of operation of Electro-Dynamometer and Induction type wattmeter, compensation, creep, error, testing, Single Phase and Polyphase Induction type Watt-hour meters. Frequency Meters: Vibrating reed type, electrical resonance type, Power Factor Meters. Text Book-1- Ch- [XVIII,XIX,XX,XXI,XXII]

### Module-II

[10 Hours]

#### University Portion(80%): (8 Hours)

Measurement of Resistance, Inductance and Capacitance: (8 Hrs)

Resistance: Measurement of Low Resistance by Kelvin's Double Bridge, Measurement of Medium Resistance, Measurement of High Resistance, Measurement of Insulating Materials, Portable Resistance Testing set (Megohmmeter), Measurement of Insulation Resistance when Power is ON, Measurement of Resistance of Earth Connections.

Inductance: Measurement of Self Inductance by Ammeter and Voltmeter, and AC Bridges (Maxwell's, Hay's, & Anderson Bridge), Measurement of Mutual Inductance by Felici's Method, and as Self Inductance.

Capacitance: Measurement of Capacitance by Ammeter and Voltmeter, and AC Bridges (Owen's, Schering & Wien's Bridge), Screening of Bridge Components and Wagner Earthing Device. Text Book-1- Ch-[VI, VII]

### Module- III

[10 Hours]

#### University Portion (80%): (8 Hours)

Galvanometer: (5 Hrs) Construction, Theory and Principle of operation of D'Arsonval, Vibration (Moving Magnet & Moving Coil types), and Ballistic Galvanometer, Influence of Resistance on Damping, Logarithmic decrement, Calibration of Galvanometers, Galvanometer Constants, Measurement of Flux and Magnetic Field by using Galvanometers.

Potentiometer: (3 Hrs) Construction, Theory and Principle of operation of DC Potentiometers (Crompton, Vernier, Constant Resistance, & Deflection Potentiometer), and AC Potentiometers (Drysdale-Tinsley & Gall-Tinsley Potentiometer). Text Book-1- Ch-[ VIII,IX]

### Module- IV

[10 Hours]

#### University Portion(80%): (8 Hours)

Current Transformer and Potential Transformer :(3 Hrs) Construction, Theory, Characteristics and Testing of CTs and PTs.

Electronic Instruments for Measuring Basic Parameters:(2 Hrs) Amplified DC Meters, AC Voltmeters using Rectifiers, True RMS Voltmeter, Considerations for choosing an Analog Voltmeter, Digital Voltmeters (Block Diagrams only), Q-meter

Oscilloscope:(3 Hrs) Block Diagrams, Delay Line, Multiple Trace, Oscilloscope Probes, Oscilloscope Techniques, Introduction to Analog and Digital Storage Oscilloscopes, Measurement of Frequency, Phase Angle, and Time Delay using Oscilloscope.

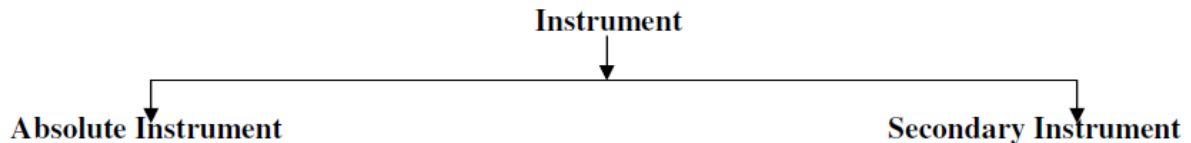
Text Book-2- Ch- [6.2 to 6.9, 7.2, 7.6, 7.7]



## MEASURING INSTRUMENTS

### 1.1 Definition of instruments

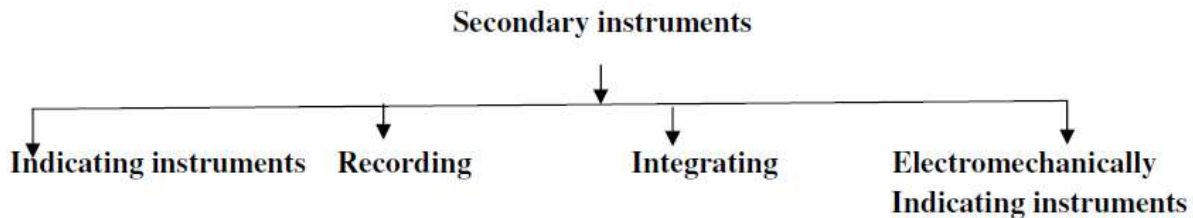
An instrument is a device in which we can determine the magnitude or value of the quantity to be measured. The measuring quantity can be voltage, current, power and energy etc. Generally instruments are classified in to two categories.



### 1.2 Absolute instrument

This instrument determines the value of the quantity to be measured directly. Generally these instruments are calibrated by comparing with another standard secondary instrument.

Examples of such instruments are voltmeter, ammeter and wattmeter etc. Practically secondary instruments are suitable for measurement.



#### 1.3.1 Indicating instrument

This instrument uses a dial and pointer to determine the value of measuring quantity. The pointer indication gives the magnitude of measuring quantity.

#### 1.3.2 Recording instrument

This type of instruments records the magnitude of the quantity to be measured continuously over a specified period of time.

#### 1.3.3 Integrating instrument

This type of instrument gives the total amount of the quantity to be measured over a specified period of time.

### 1.3.4 Electromechanical indicating instrument

For satisfactory operation electromechanical indicating instrument, three forces are necessary. They are

- (a) Deflecting force
- (b) Controlling force
- (c) Damping force

### 1.4 Deflecting force

When there is no input signal to the instrument, the pointer will be at its zero position. To deflect the pointer from its zero position, a force is necessary which is known as deflecting force. A system which produces the deflecting force is known as a deflecting system. Generally a deflecting system converts an electrical signal to a mechanical force.

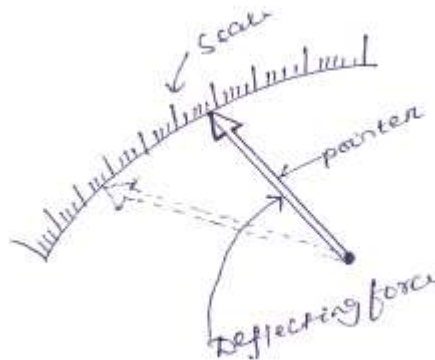


Fig.1:Pointer scale

### 1.4.1 Magnitude effect

When a current passes through the coil (Fig.1.2), it produces an imaginary bar magnet. When a soft-iron piece is brought near this coil it is magnetized. Depending upon the current direction the poles are produced in such a way that there will be a force of attraction between the coil and the soft iron piece. This principle is used in moving iron attraction type instrument.

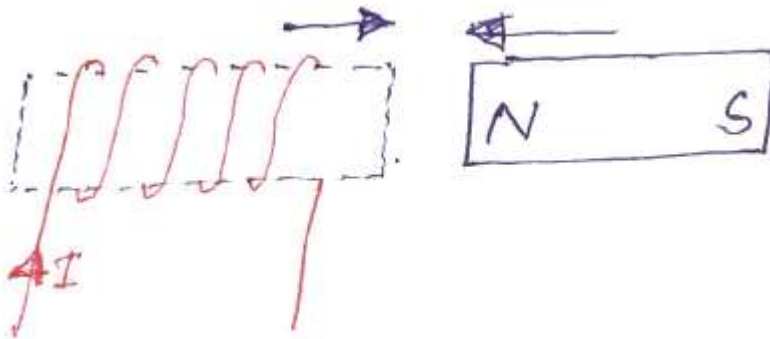


Fig.2:

If two soft iron pieces are placed near a current carrying coil there will be a force of repulsion between the two soft iron pieces. This principle is utilized in the moving iron repulsion type instrument.

#### 1.4.2 Force between a permanent magnet and a current carrying coil

When a current carrying coil is placed under the influence of magnetic field produced by a permanent magnet and a force is produced between them. This principle is utilized in the moving coil type instrument.

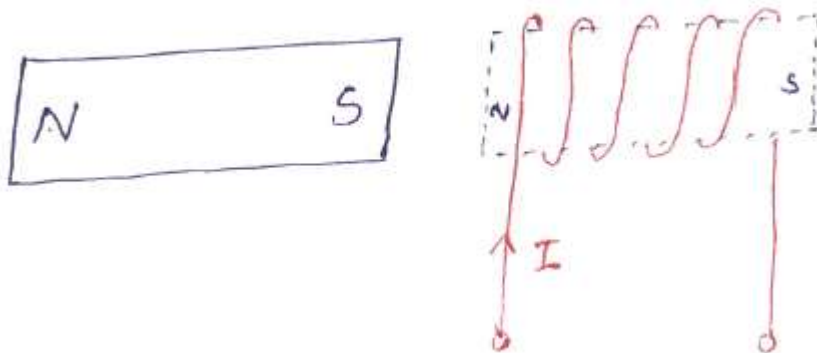


Fig. 1.3

#### 1.4.3 Force between two current carrying coil

When two current carrying coils are placed closer to each other there will be a force of repulsion between them. If one coil is movable and other is fixed, the movable coil will move away from the fixed one. This principle is utilized in electrodynamicometer type instrument.

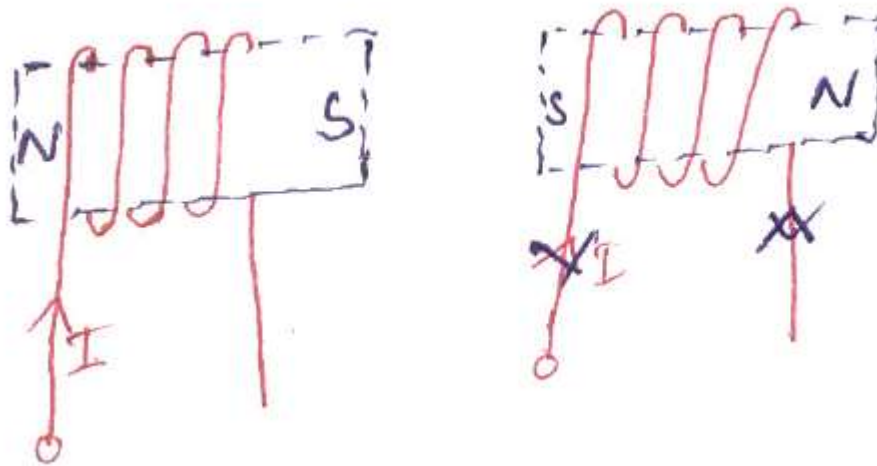


Fig. 1.4

### 1.5 Controlling force

To make the measurement indicated by the pointer definite (constant) a force is necessary which will be acting in the opposite direction to the deflecting force. This force is known as controlling force. A system which produces this force is known as a controlled system. When the external signal to be measured by the instrument is removed, the pointer should return back to the zero position. This is possibly due to the controlling force and the pointer will be indicating a steady value when the deflecting torque is equal to controlling torque.

$$T_d = T_c \quad (1.1)$$

#### 1.5.1 Spring control

Two springs are attached on either end of spindle (Fig. 1.5). The spindle is placed in jeweled bearing, so that the frictional force between the pivot and spindle will be minimum. Two springs are provided in opposite direction to compensate the temperature error. The spring is made of phosphorous bronze.

When a current is supply, the pointer deflects due to rotation of the spindle. While spindle is rotate, the spring attached with the spindle will oppose the movements of the pointer. The torque produced by the spring is directly proportional to the pointer deflection  $\theta$ .

$$T_c \propto \theta \quad (1.2)$$

The deflecting torque produced  $T_d$  proportional to 'I'. When  $T_c = T_d$ , the pointer will come to a steady position. Therefore

$\theta \propto I$

(1.3)

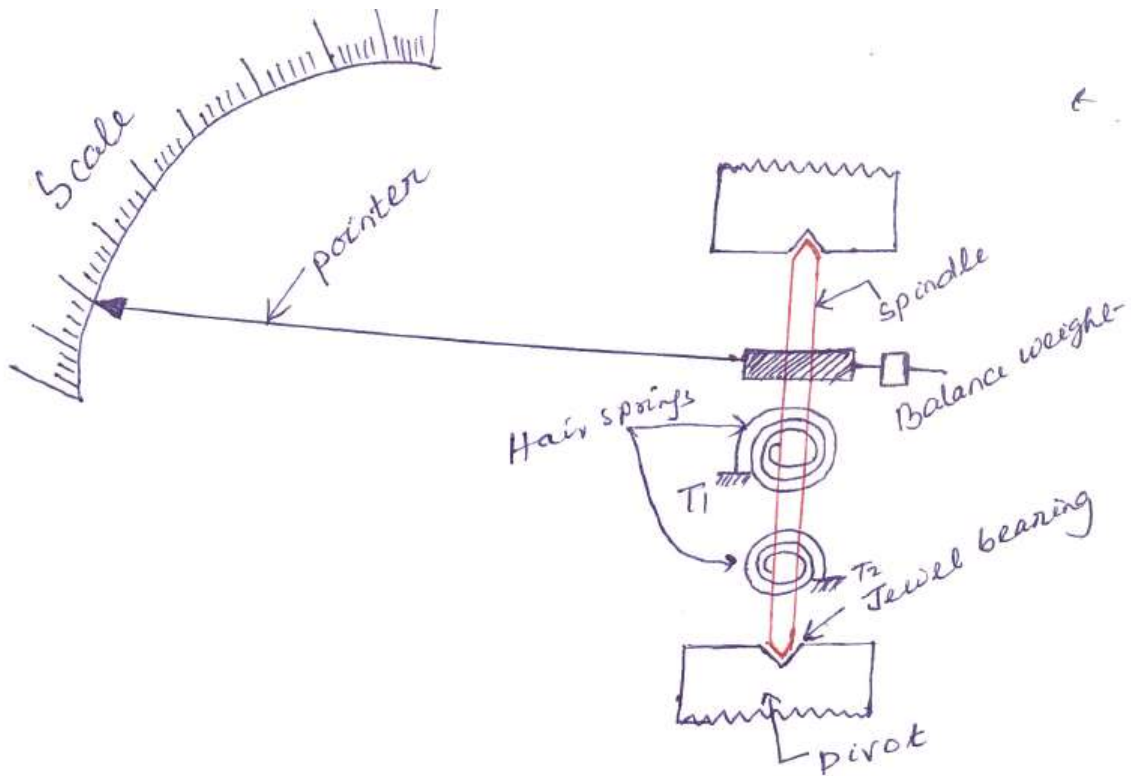


Fig. 1.5

Since,  $\theta$  and  $I$  are directly proportional to the scale of such instrument which uses spring controlled is uniform.

## 1.6 Damping force

The deflection torque and controlling torque produced by systems are electro mechanical. Due to inertia produced by this system, the pointer oscillates about its final steady position before coming to rest. The time required to take the measurement is more. To damp out the oscillation as quickly as possible, a damping force is necessary. This force is produced by different systems.

- (a) Air friction damping
- (b) Fluid friction damping
- (c) Eddy current damping

### 1.6.1 Air friction damping

The piston is mechanically connected to a spindle through the connecting rod (Fig. 1.6). The pointer is fixed to the spindle and moves over a calibrated dial. When the pointer oscillates in the clockwise direction, the piston goes inside and the cylinder gets compressed. The air pushes the piston upwards and the pointer tends to move in the anticlockwise direction.

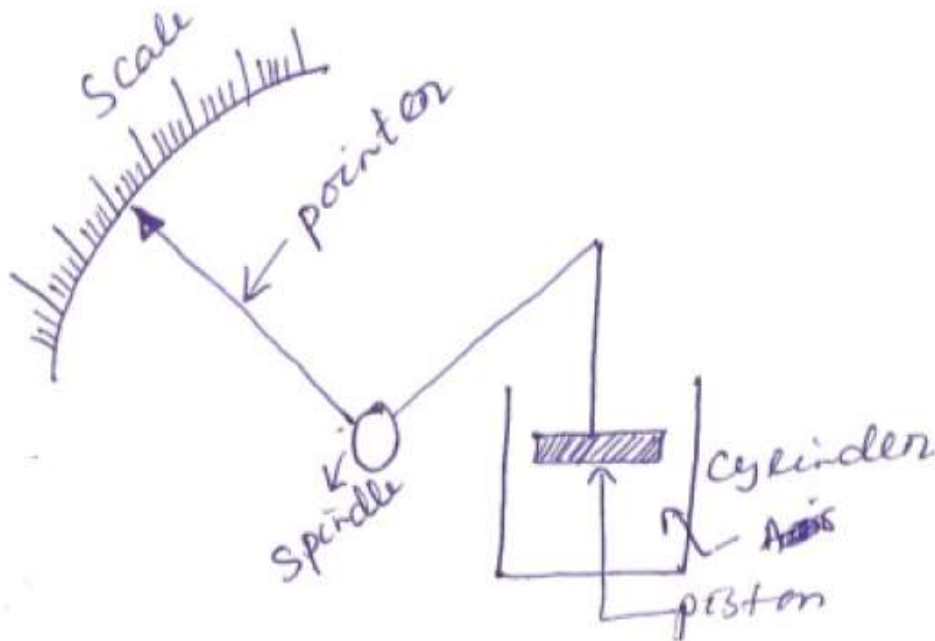


Fig. 1.6



If the pointer oscillates in anticlockwise direction the piston moves away and the pressure of the air inside cylinder gets reduced. The external pressure is more than that of the internal pressure. Therefore the piston moves down wards. The pointer tends to move in clock wise direction.

### 1.6.2 Eddy current damping

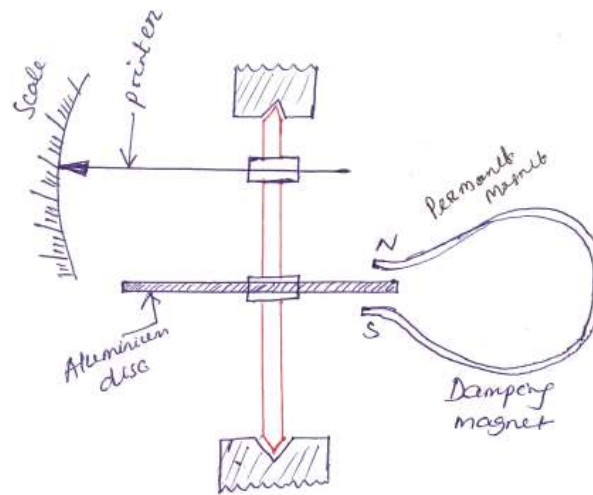


Fig. 1.6 Disc type

An aluminum circular disc is fixed to the spindle (Fig. 1.6). This disc is made to move in the magnetic field produced by a permanent magnet.

When the disc oscillates it cuts the magnetic flux produced by damping magnet. An emf is induced in the circular disc by Faraday's law. Eddy currents are established in the disc since it has several closed paths. By Lenz's law, the current carrying disc produces a force in a direction opposite to oscillating force. The damping force can be varied by varying the projection of the magnet over the circular disc.

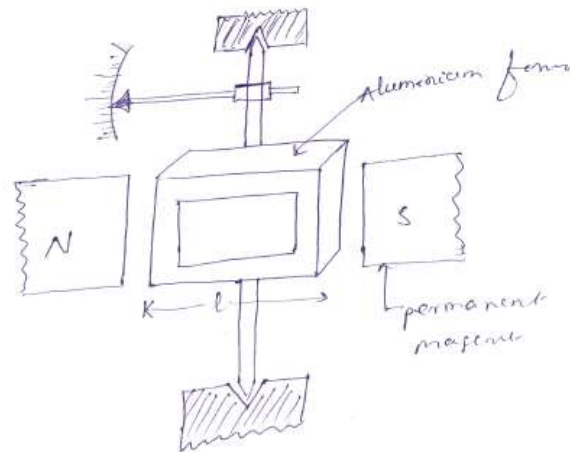


Fig. 1.6 Rectangular type

### 1.7 Permanent Magnet Moving Coil (PMMC) instrument

One of the most accurate types of instrument used for D.C. measurements is PMMC instrument.

**Construction:** A permanent magnet is used in this type of instrument. An aluminum former is provided in the cylindrical space between two poles of the permanent magnet (Fig. 1.7). Coils are wound on the aluminum former which is connected with the spindle. This spindle is supported with jeweled bearings. Two springs are attached on either end of the spindle. The terminals of the moving coils are connected to the springs. Therefore the current flows through spring 1, moving coil and spring 2.

**Damping:** Eddy current damping is used. This is produced by an aluminum former.

**Control:** Spring control is used.

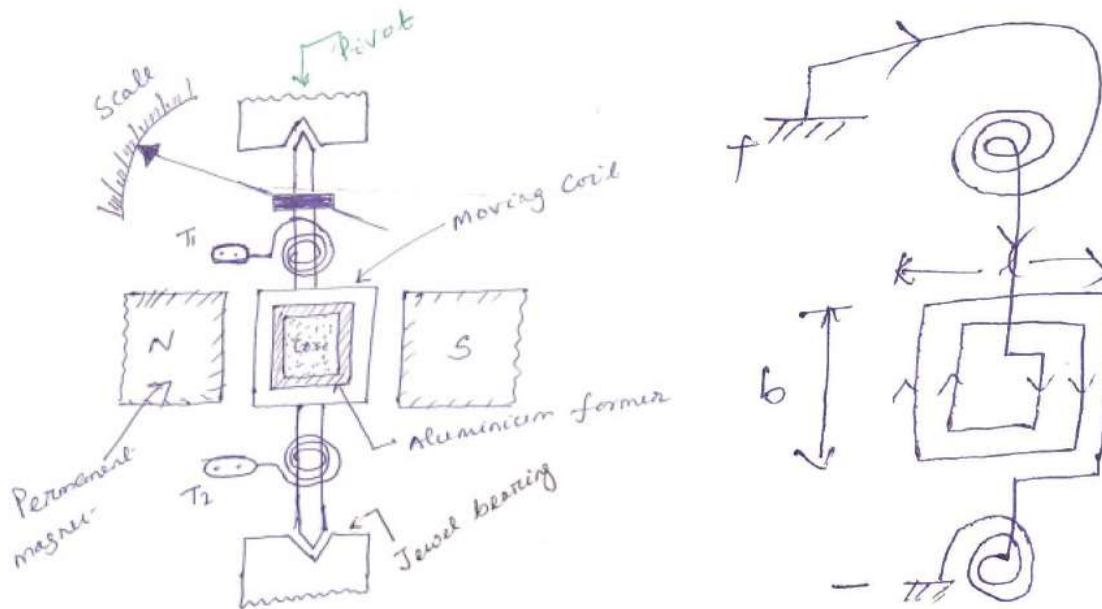


Fig. 1.7

**Principle of operation**

When D.C. supply is given to the moving coil, D.C. current flows through it. When the current carrying coil is kept in the magnetic field, it experiences a force. This force produces a torque and the former rotates. The pointer is attached with the spindle. When the former rotates, the pointer moves over the calibrated scale. When the polarity is reversed a torque is produced in the opposite direction. The mechanical stopper does not allow the deflection in the opposite direction. Therefore the polarity should be maintained with PMMC instrument.

If A.C. is supplied, a reversing torque is produced. This cannot produce a continuous deflection. Therefore this instrument cannot be used in A.C.

**Torque developed by PMMC**

Let  $T_d$  = deflecting torque

$T_C$  = controlling torque

$\theta$  = angle of deflection

K = spring constant

b = width of the coil



$l$ =height of the coil or length of coil

$N$ =No. of turns

$I$ =current

$B$ =Flux density

$A$ =area of the coil

The force produced in the coil is given by

$$F = BIL \sin \theta \quad (1.4)$$

When  $\theta = 90^\circ$

$$\text{For } N \text{ turns, } F = NBIL \quad (1.5)$$

$$\text{Torque produced } T_d = F \times \perp_r \text{ distance} \quad (1.6)$$

$$T_d = NBIL \times b = BINA \quad (1.7)$$

$$T_d = BANl \quad (1.8)$$

$$T_d \propto I \quad (1.9)$$

#### Advantages

- ✓ Torque/weight is high
- ✓ Power consumption is less
- ✓ Scale is uniform
- ✓ Damping is very effective
- ✓ Since operating field is very strong, the effect of stray field is negligible
- ✓ Range of instrument can be extended

#### Disadvantages

- ✓ Use only for D.C.
- ✓ Cost is high
- ✓ Error is produced due to ageing effect of PMMC
- ✓ Friction and temperature error are present

### 1.7.1 Extension of range of PMMC instrument

#### Case-I: Shunt

A low shunt resistance connected in parallel with the ammeter to extend the range of current. Large current can be measured using low current rated ammeter by using a shunt.

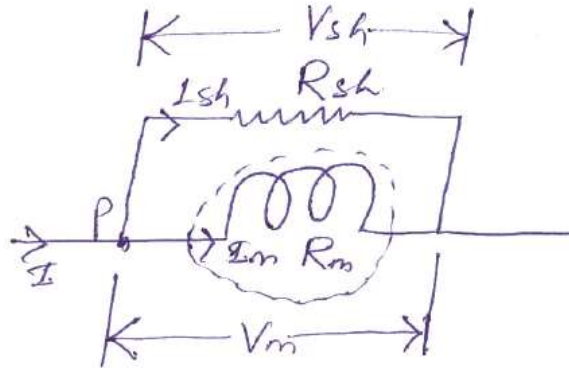


Fig. 1.8

Let  $R_m$  = Resistance of meter

$R_{sh}$  = Resistance of shunt

$I_m$  = Current through meter

$I_{sh}$  = current through shunt

$I$  = current to be measure

$$\therefore V_m = V_{sh} \quad (1.10)$$

$$I_m R_m = I_{sh} R_{sh}$$

$$\frac{I_m}{I_{sh}} = \frac{R_{sh}}{R_m} \quad (1.11)$$

Apply KCL at 'P'  $I = I_m + I_{sh}$  (1.12)

Eq<sup>n</sup> (1.12)  $\div$  by  $I_m$

$$\frac{I}{I_m} = 1 + \frac{I_{sh}}{I_m} \quad (1.13)$$

$$\frac{I}{I_m} = 1 + \frac{R_m}{R_{sh}} \quad (1.14)$$

$$\therefore I = I_m \left( 1 + \frac{R_m}{R_{sh}} \right) \quad (1.15)$$

$\left( 1 + \frac{R_m}{R_{sh}} \right)$  is called multiplication factor

Shunt resistance is made of manganin. This has least thermoelectric emf. The change in resistance, due to change in temperature is negligible.

### Case (II): Multiplier

A large resistance is connected in series with voltmeter is called multiplier (Fig. 1.9). A large voltage can be measured using a voltmeter of small rating with a multiplier.

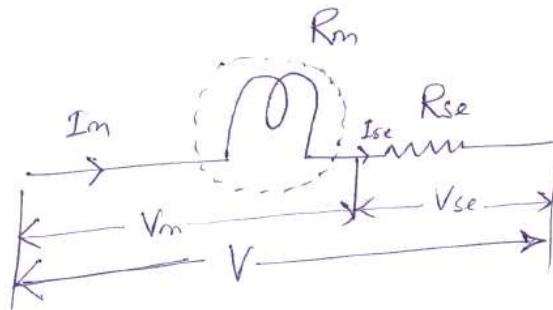


Fig. 1.9

Let  $R_m$  = resistance of meter

$R_{se}$  = resistance of multiplier

$V_m$  = Voltage across meter

$V_{se}$  = Voltage across series resistance

$V$  = voltage to be measured

$$I_m = I_{se} \quad (1.16)$$

$$\frac{V_m}{R_m} = \frac{V_{se}}{R_{se}} \quad (1.17)$$

$$\therefore \frac{V_{se}}{V_m} = \frac{R_{se}}{R_m} \quad (1.18)$$

$$\text{Apply KVL, } V = V_m + V_{se} \quad (1.19)$$

$$\text{Eq}^n (1.19) \div V_m$$

$$\frac{V}{V_m} = 1 + \frac{V_{se}}{V_m} = \left( 1 + \frac{R_{se}}{R_m} \right) \quad (1.20)$$

$$\therefore V = V_m \left( 1 + \frac{R_{se}}{R_m} \right) \quad (1.21)$$

$$\left( 1 + \frac{R_{se}}{R_m} \right) \rightarrow \text{Multiplication factor}$$

## 1.8 Moving Iron (MI) instruments

One of the most accurate instrument used for both AC and DC measurement is moving iron instrument. There are two types of moving iron instrument.

- Attraction type
- Repulsion type

### 1.8.1 Attraction type M.I. instrument

**Construction:** The moving iron fixed to the spindle is kept near the hollow fixed coil (Fig. 1.10). The pointer and balance weight are attached to the spindle, which is supported with jeweled bearing. Here air friction damping is used.

#### Principle of operation

The current to be measured is passed through the fixed coil. As the current is flow through the fixed coil, a magnetic field is produced. By magnetic induction the moving iron gets magnetized. The north pole of moving coil is attracted by the south pole of fixed coil. Thus the deflecting force is produced due to force of attraction. Since the moving iron is attached with the spindle, the spindle rotates and the pointer moves over the calibrated scale. But the force of attraction depends on the current flowing through the coil.

#### Torque developed by M.I

Let '  $\theta$  ' be the deflection corresponding to a current of 'i' amp

Let the current increases by di, the corresponding deflection is '  $\theta + d\theta$  '

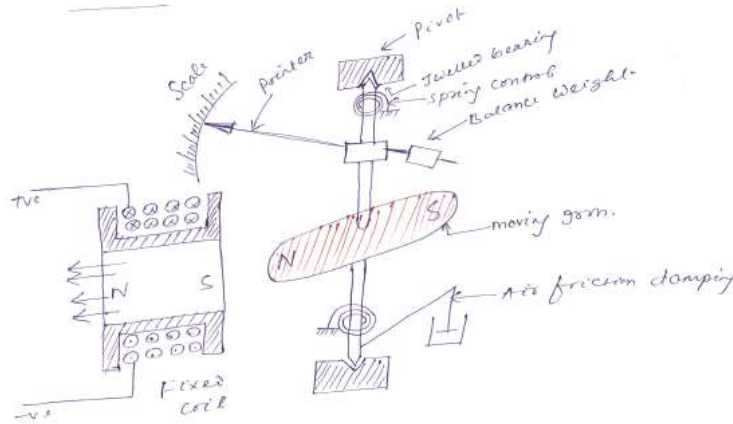


Fig. 1.10

There is change in inductance since the position of moving iron change w.r.t the fixed electromagnets.

Let the new inductance value be ' $L+dL$ '. The current change by ' $di$ ' is  $dt$  seconds.

Let the emf induced in the coil be ' $e$ ' volt.

$$e = \frac{d}{dt}(Li) = L \frac{di}{dt} + i \frac{dL}{dt} \quad (1.22)$$

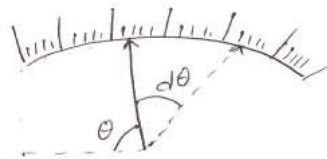
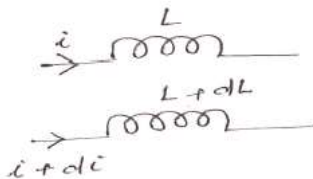
Multiplying by ' $idt$ ' in equation (1.22)

$$e \times idt = L \frac{di}{dt} \times idt + i \frac{dL}{dt} \times idt \quad (1.23)$$

$$e \times idt = Lidi + i^2 dL \quad (1.24)$$

Eq<sup>n</sup> (1.24) gives the energy is used in to two forms. Part of energy is stored in the inductance.

Remaining energy is converted in to mechanical energy which produces deflection.





Change in energy stored=Final energy-initial energy stored

$$\begin{aligned}
 &= \frac{1}{2}(L + dL)(i + di)^2 - \frac{1}{2}Li^2 \\
 &= \frac{1}{2}\{(L + dL)(i^2 + di^2 + 2idi) - Li^2\} \\
 &= \frac{1}{2}\{(L + dL)(i^2 + 2idi) - Li^2\} \\
 &= \frac{1}{2}\{Li^2 + 2Lidi + i^2dL + 2ididL - Li^2\} \\
 &= \frac{1}{2}\{2Lidi + i^2dL\} \\
 &= Lidi + \frac{1}{2}i^2dL \tag{1.25}
 \end{aligned}$$

Mechanical work to move the pointer by  $d\theta$

$$= T_d d\theta \tag{1.26}$$

By law of conservation of energy,

Electrical energy supplied=Increase in stored energy+ mechanical work done.

Input energy= Energy stored + Mechanical energy

$$Lidi + i^2dL = Lidi + \frac{1}{2}i^2dL + T_d d\theta \tag{1.27}$$

$$\frac{1}{2}i^2dL = T_d d\theta \tag{1.28}$$

$$T_d = \frac{1}{2}i^2 \frac{dL}{d\theta} \tag{1.29}$$

At steady state condition  $T_d = T_C$

$$\frac{1}{2}i^2 \frac{dL}{d\theta} = K\theta \tag{1.30}$$

$$\theta = \frac{1}{2K}i^2 \frac{dL}{d\theta} \tag{1.31}$$

$$\theta \propto i^2 \tag{1.32}$$

When the instruments measure AC,  $\theta \propto i_{rms}^2$

Scale of the instrument is non uniform.

### **Advantages**

- ✓ MI can be used in AC and DC
- ✓ It is cheap
- ✓ Supply is given to a fixed coil, not in moving coil.
- ✓ Simple construction
- ✓ Less friction error.

### **Disadvantages**

- ✓ It suffers from eddy current and hysteresis error
- ✓ Scale is not uniform
- ✓ It consumed more power
- ✓ Calibration is different for AC and DC operation

### **1.8.2 Repulsion type moving iron instrument**

**Construction:** The repulsion type instrument has a hollow fixed iron attached to it (Fig. 1.12). The moving iron is connected to the spindle. The pointer is also attached to the spindle in supported with jeweled bearing.

**Principle of operation:** When the current flows through the coil, a magnetic field is produced by it. So both fixed iron and moving iron are magnetized with the same polarity, since they are kept in the same magnetic field. Similar poles of fixed and moving iron get repelled. Thus the deflecting torque is produced due to magnetic repulsion. Since moving iron is attached to spindle, the spindle will move. So that pointer moves over the calibrated scale.

**Damping:** Air friction damping is used to reduce the oscillation.

**Control:** Spring control is used.

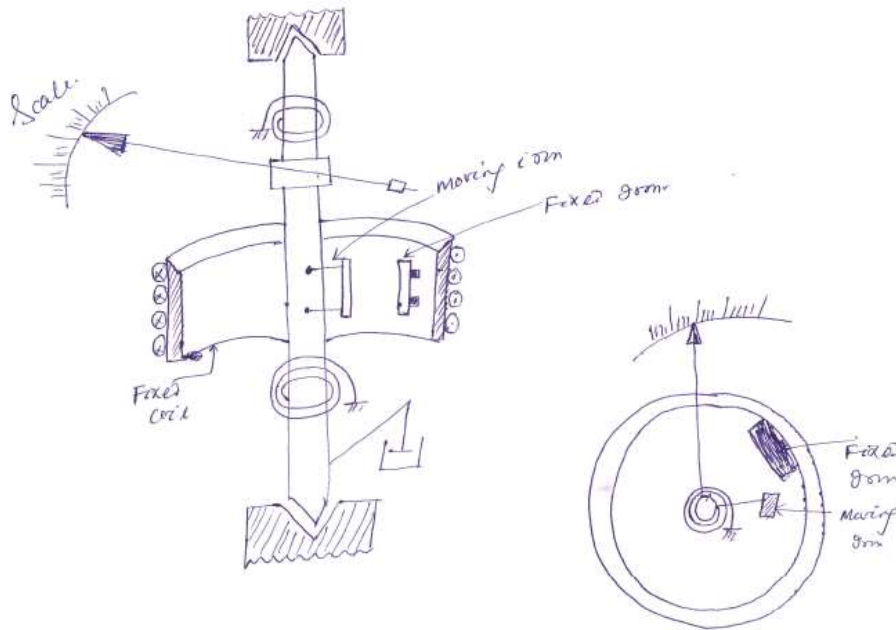


Fig. 1.12

**1.9 Dynamometer (or) Electromagnetic moving coil instrument (EMMC)**

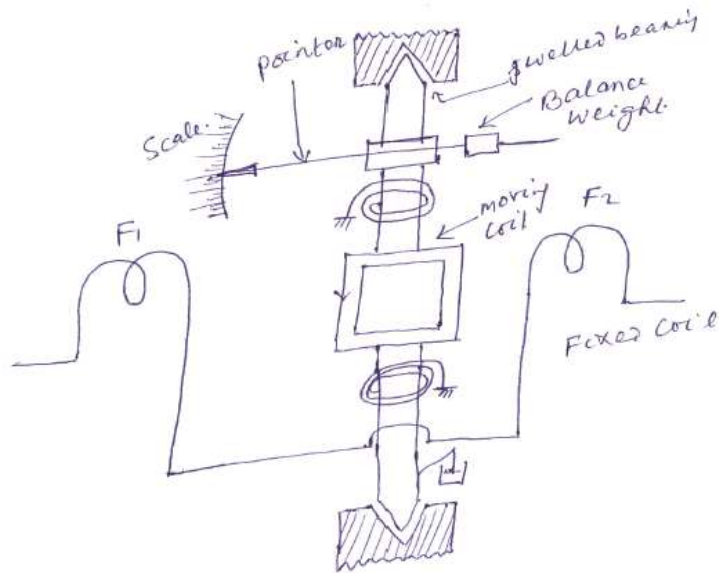


Fig. 1.13

This instrument can be used for the measurement of voltage, current and power. The difference between the PMMC and dynamometer type instrument is that the permanent magnet is replaced by an electromagnet.

**Construction:** A fixed coil is divided into two equal halves. The moving coil is placed between the two halves of the fixed coil. Both the fixed and moving coils are air-cored. So that the hysteresis effect will be zero. The pointer is attached with the spindle. In a non-metallic former the moving coil is wound.

**Control:** Spring control is used.

**Damping:** Air friction damping is used.

**Principle of operation:**

When the current flows through the fixed coil, it produces a magnetic field, whose flux density is proportional to the current through the fixed coil. The moving coil is kept in between the fixed coil. When the current passes through the moving coil, a magnetic field is produced by this coil.

The magnetic poles are produced in such a way that the torque produced on the moving coil deflects the pointer over the calibrated scale. This instrument works on AC and DC. When AC voltage is applied, alternating current flows through the fixed coil and moving coil. When the current in the fixed coil reverses, the current in the moving coil also reverses. Torque remains in the same direction. Since the current  $i_1$  and  $i_2$  reverse simultaneously. This is because the fixed and moving coils are either connected in series or parallel.

**Torque developed by EMMC**

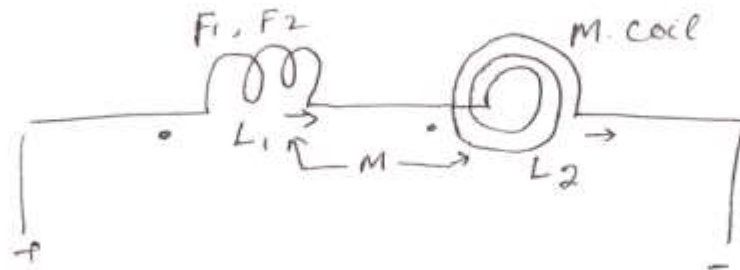


Fig. 1.14



Let

$L_1$ =Self inductance of fixed coil

$L_2$ = Self inductance of moving coil

$M$ =mutual inductance between fixed coil and moving coil

$i_1$ =current through fixed coil

$i_2$ =current through moving coil

Total inductance of system,

$$L_{total} = L_1 + L_2 + 2M \quad (1.33)$$

But we know that in case of M.I

$$T_d = \frac{1}{2} i^2 \frac{d(L)}{d\theta} \quad (1.34)$$

$$T_d = \frac{1}{2} i^2 \frac{d}{d\theta} (L_1 + L_2 + 2M) \quad (1.35)$$

The value of  $L_1$  and  $L_2$  are independent of ' $\theta$ ' but ' $M$ ' varies with  $\theta$

$$T_d = \frac{1}{2} i^2 \times 2 \frac{dM}{d\theta} \quad (1.36)$$

$$T_d = i^2 \frac{dM}{d\theta} \quad (1.37)$$

If the coils are not connected in series  $i_1 \neq i_2$

$$\therefore T_d = i_1 i_2 \frac{dM}{d\theta} \quad (1.38)$$

$$T_C = T_d \quad (1.39)$$

$$\therefore \theta = \frac{i_1 i_2}{K} \frac{dM}{d\theta} \quad (1.40)$$

Hence the deflection of pointer is proportional to the current passing through fixed coil and moving coil.

### 1.9.1 Extension of EMMC instrument

#### Case-I Ammeter connection

Fixed coil and moving coil are connected in parallel for ammeter connection. The coils are designed such that the resistance of each branch is same.

Therefore

$$I_1 = I_2 = I$$

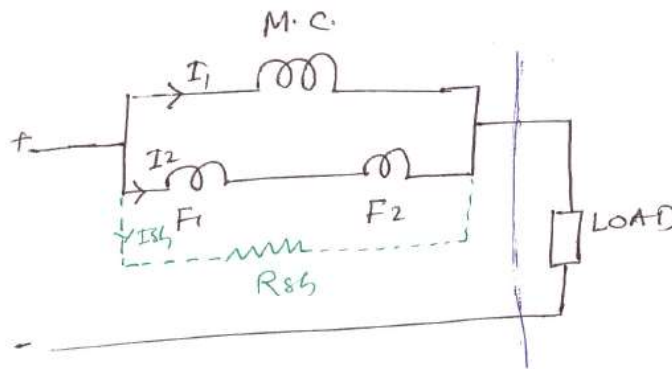


Fig. 1.15

To extend the range of current a shunt may be connected in parallel with the meter. The value  $R_{sh}$  is designed such that equal current flows through moving coil and fixed coil.

$$\therefore T_d = I_1 I_2 \frac{dM}{d\theta} \quad (1.41)$$

$$\text{Or } \therefore T_d = I^2 \frac{dM}{d\theta} \quad (1.42)$$

$$T_C = K\theta \quad (1.43)$$

$$\theta = \frac{I^2}{K} \frac{dM}{d\theta} \quad (1.44)$$

$$\therefore \theta \propto I^2 \text{ (Scale is not uniform)} \quad (1.45)$$

#### Case-II Voltmeter connection

Fixed coil and moving coil are connected in series for voltmeter connection. A multiplier may be connected in series to extent the range of voltmeter.

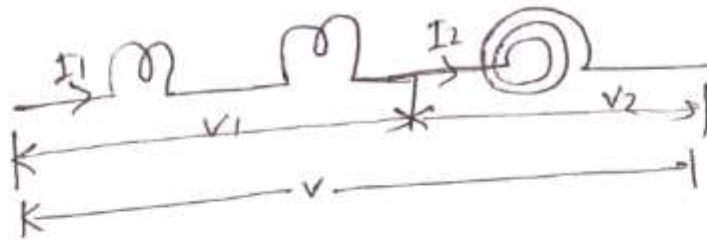


Fig. 1.16

$$I_1 = \frac{V_1}{Z_1}, I_2 = \frac{V_2}{Z_2} \quad (1.46)$$

$$T_d = \frac{V_1}{Z_1} \times \frac{V_2}{Z_2} \times \frac{dM}{d\theta} \quad (1.47)$$

$$T_d = \frac{K_1 V}{Z_1} \times \frac{K_2 V}{Z_2} \times \frac{dM}{d\theta} \quad (1.48)$$

$$T_d = \frac{KV^2}{Z_1 Z_2} \times \frac{dM}{d\theta} \quad (1.49)$$

$$T_d \propto V^2 \quad (1.50)$$

$$\therefore \theta \propto V^2 \text{ (Scale is not uniform)} \quad (1.51)$$

**Case-III As wattmeter**

When the two coils are connected to parallel, the instrument can be used as a wattmeter. Fixed coil is connected in series with the load. Moving coil is connected in parallel with the load. The moving coil is known as voltage coil or pressure coil and fixed coil is known as current coil.

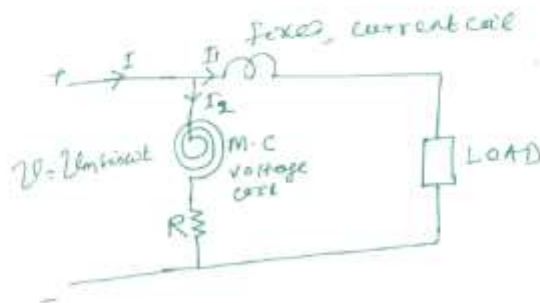


Fig. 1.17

Assume that the supply voltage is sinusoidal. If the impedance of the coil is neglected in comparison with the resistance 'R'. The current,

$$I_2 = \frac{v_m \sin wt}{R} \quad (1.52)$$

Let the phase difference between the currents  $I_1$  and  $I_2$  is  $\phi$

$$I_1 = I_m \sin(wt - \phi) \quad (1.53)$$

$$T_d = I_1 I_2 \frac{dM}{d\theta} \quad (1.54)$$

$$T_d = I_m \sin(wt - \phi) \times \frac{V_m \sin wt}{R} \frac{dM}{d\theta} \quad (1.55)$$

$$T_d = \frac{1}{R} (I_m V_m \sin wt \sin(wt - \phi)) \frac{dM}{d\theta} \quad (1.56)$$

$$T_d = \frac{1}{R} I_m V_m \sin wt \cdot \sin(wt - \phi) \frac{dM}{d\theta} \quad (1.57)$$

The average deflecting torque

$$(T_d)_{avg} = \frac{1}{2\pi} \int_0^{2\pi} T_d \times d(wt) \quad (1.58)$$

$$(T_d)_{avg} = \frac{1}{2\pi} \int_0^{2\pi} \frac{1}{R} \times I_m V_m \sin wt \cdot \sin(wt - \phi) \frac{dM}{d\theta} \times d(wt) \quad (1.59)$$

$$(T_d)_{avg} = \frac{V_m I_m}{2 \times 2\pi} \times \frac{1}{R} \times \frac{dM}{d\theta} \left[ \int \{ \cos \phi - \cos(2wt - \phi) \} dwt \right] \quad (1.60)$$

$$(T_d)_{avg} = \frac{V_m I_m}{4\pi R} \times \frac{dM}{d\theta} \left[ \int_0^{2\pi} \cos \phi \cdot dwt - \int_0^{2\pi} \cos(2wt - \phi) \cdot dwt \right] \quad (1.61)$$

$$(T_d)_{avg} = \frac{V_m I_m}{4\pi R} \times \frac{dM}{d\theta} [\cos \phi [wt]_0^{2\pi}] \quad (1.62)$$

$$(T_d)_{avg} = \frac{V_m I_m}{4\pi R} \times \frac{dM}{d\theta} [\cos \phi (2\pi - 0)] \quad (1.63)$$

$$(T_d)_{avg} = \frac{V_m I_m}{2} \times \frac{1}{R} \times \frac{dM}{d\theta} \times \cos \phi \quad (1.64)$$

$$(T_d)_{avg} = V_{rms} \times I_{rms} \times \cos \phi \times \frac{1}{R} \times \frac{dM}{d\theta} \quad (1.65)$$





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$$(T_d)_{avg} \propto KVI \cos \phi \quad (1.66)$$

$$T_C \propto \theta \quad (1.67)$$

$$\theta \propto KVI \cos \phi \quad (1.68)$$

$$\theta \propto VI \cos \phi \quad (1.69)$$

### Advantages

- ✓ It can be used for voltmeter, ammeter and wattmeter
- ✓ Hysteresis error is nill
- ✓ Eddy current error is nill
- ✓ Damping is effective
- ✓ It can be measure correctively and accurately the rms value of the voltage

### Disadvantages

- ✓ Scale is not uniform
- ✓ Power consumption is high(because of high resistance )
- ✓ Cost is more
- ✓ Error is produced due to frequency, temperature and stray field.
- ✓ Torque/weight is low.(Because field strength is very low)

### **Errors in PMMC**

- ✓ The permanent magnet produced error due to ageing effect. By heat treatment, this error can be eliminated.
- ✓ The spring produces error due to ageing effect. By heat treating the spring the error can be eliminated.
- ✓ When the temperature changes, the resistance of the coil vary and the spring also produces error in deflection. This error can be minimized by using a spring whose temperature co-efficient is very low.

### **1.10 Difference between attraction and repulsion type instrument**

An attraction type instrument will usually have a lower inductance, compare to repulsion type instrument. But in other hand, repulsion type instruments are more suitable for economical production in manufacture and nearly uniform scale is more easily obtained. They are therefore much more common than attraction type.



**Example: 1.1**

A PMMC ammeter has the following specification

Coil dimension are  $1\text{cm} \times 1\text{cm}$ . Spring constant is  $0.15 \times 10^{-6} \text{ N-m/rad}$ , Flux density is  $1.5 \times 10^{-3} \text{ wb/m}^2$ . Determine the no. of turns required to produce a deflection of  $90^\circ$  when a current 2mA flows through the coil.

**Solution:**

At steady state condition  $T_d = T_C$

$$BANl = K\theta$$

$$\Rightarrow N = \frac{K\theta}{BAI}$$

$$A = 1 \times 10^{-4} \text{ m}^2$$

$$K = 0.15 \times 10^{-6} \frac{\text{N-m}}{\text{rad}}$$

$$B = 1.5 \times 10^{-3} \text{ wb/m}^2$$

$$I = 2 \times 10^{-3} \text{ A}$$

$$\theta = 90^\circ = \frac{\pi}{2} \text{ rad}$$

$$N = 785 \text{ ans.}$$

## AC BRIDGES

### 2.1 General form of A.C. bridge

AC bridge are similar to D.C. bridge in topology (way of connecting). It consists of four arm AB, BC, CD and DA. Generally the impedance to be measured is connected between 'A' and 'B'. A detector is connected between 'B' and 'D'. The detector is used as null deflection instrument. Some of the arms are variable element. By varying these elements, the potential values at 'B' and 'D' can be made equal. This is called balancing of the bridge.

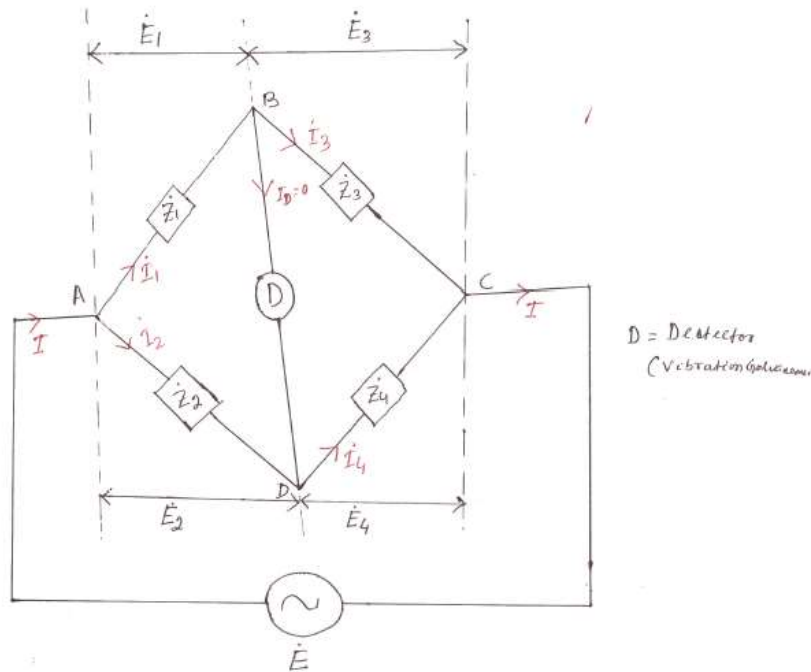


Fig. 2.1 General form of A.C. bridge

At the balance condition, the current through detector is zero.

$$\therefore \dot{I}_1 = \dot{I}_3$$

$$\dot{I}_2 = \dot{I}_4$$

$$\therefore \frac{\dot{I}_1}{\dot{I}_2} = \frac{\dot{I}_3}{\dot{I}_4}$$

(2.1)



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At balance condition,

Voltage drop across 'AB'=voltage drop across 'AD'.

$$\dot{E}_1 = \dot{E}_2$$

$$\therefore \dot{I}_1 \dot{Z}_1 = \dot{I}_2 \dot{Z}_2 \quad (2.2)$$

Similarly, Voltage drop across 'BC'=voltage drop across 'DC'

$$\dot{E}_3 = \dot{E}_4$$

$$\therefore \dot{I}_3 \dot{Z}_3 = \dot{I}_4 \dot{Z}_4 \quad (2.3)$$

From Eqn. (2.2), we have  $\therefore \frac{\dot{I}_1}{\dot{I}_2} = \frac{\dot{Z}_2}{\dot{Z}_1}$  (2.4)

From Eqn. (2.3), we have  $\therefore \frac{\dot{I}_3}{\dot{I}_4} = \frac{\dot{Z}_4}{\dot{Z}_3}$  (2.5)

From equation -2.1, it can be seen that, equation -2.4 and equation-2.5 are equal.

$$\therefore \frac{\dot{Z}_2}{\dot{Z}_1} = \frac{\dot{Z}_4}{\dot{Z}_3}$$

$$\therefore \dot{Z}_1 \dot{Z}_4 = \dot{Z}_2 \dot{Z}_3$$

Products of impedances of opposite arms are equal.

$$\therefore |Z_1| \angle \theta_1 |Z_4| \angle \theta_4 = |Z_2| \angle \theta_2 |Z_3| \angle \theta_3$$

$$\Rightarrow |Z_1| |Z_4| \angle \theta_1 + \theta_4 = |Z_2| |Z_3| \angle \theta_2 + \theta_3$$

$$|Z_1| |Z_4| = |Z_2| |Z_3|$$

$$\theta_1 + \theta_4 = \theta_2 + \theta_3$$



- \* For balance condition, magnitude on either side must be equal.
- \* Angle on either side must be equal.

### **Summary**

For balance condition,

- $\dot{I}_1 = \dot{I}_3, \dot{I}_2 = \dot{I}_4$
- $|Z_1||Z_4| = |Z_2||Z_3|$
- $\theta_1 + \theta_4 = \theta_2 + \theta_3$
- $\dot{E}_1 = \dot{E}_2 \quad \& \quad \dot{E}_3 = \dot{E}_4$

### **2.2 Types of detector**

The following types of instruments are used as detector in A.C. bridge.

- Vibration galvanometer
- Head phones (speaker)
- Tuned amplifier

#### **2.2.1 Vibration galvanometer**

Between the point 'B' and 'D' a vibration galvanometer is connected to indicate the bridge balance condition. This A.C. galvanometer which works on the principle of resonance. The A.C. galvanometer shows a dot, if the bridge is unbalanced.

#### **2.2.2 Head phones**

Two speakers are connected in parallel in this system. If the bridge is unbalanced, the speaker produced more sound energy. If the bridge is balanced, the speaker do not produced any sound energy.

#### **2.2.3 Tuned amplifier**

If the bridge is unbalanced the output of tuned amplifier is high. If the bridge is balanced, output of amplifier is zero.







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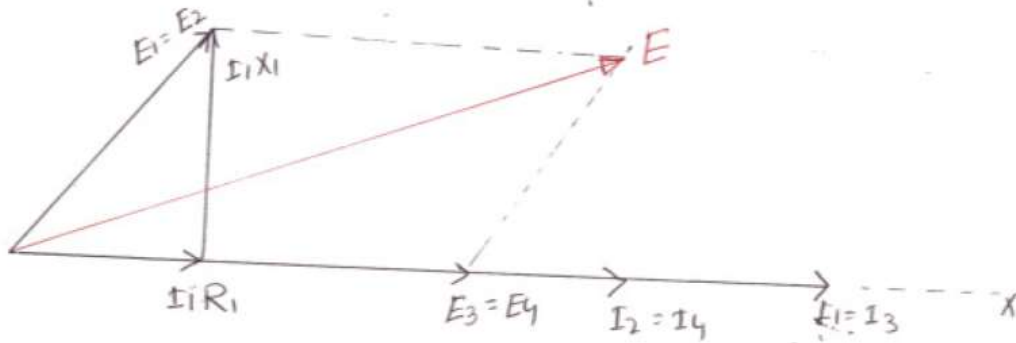


Fig 2.3 Phasor diagram of Maxwell's inductance bridge

At balance condition,  $\dot{Z}_1 \dot{Z}_4 = \dot{Z}_2 \dot{Z}_3$

$$(R_1 + jXL_1)R_4 = (R_2 + jXL_2)R_3$$

$$(R_1 + j\omega L_1)R_4 = (R_2 + j\omega L_2)R_3$$

$$R_1R_4 + j\omega L_1R_4 = R_2R_3 + j\omega L_2R_3$$

Comparing real part,

$$R_1R_4 = R_2R_3$$

$$\therefore R_1 = \frac{R_2R_3}{R_4} \quad (2.6)$$

Comparing the imaginary parts,

$$\omega L_1R_4 = \omega L_2R_3$$

$$L_1 = \frac{L_2R_3}{R_4} \quad (2.7)$$

$$Q\text{-factor of choke, } Q = \frac{\omega L_1}{R_1} = \frac{\omega L_2 R_3 R_4}{R_4 R_2 R_3}$$

$$Q = \frac{\omega L_2}{R_2} \quad (2.8)$$

### Advantages

- ✓ Expression for  $R_1$  and  $L_1$  are simple.
- ✓ Equations are simple
- ✓ They do not depend on the frequency (as  $\omega$  is cancelled)
- ✓  $R_1$  and  $L_1$  are independent of each other.

### Disadvantages

- ✓ Variable inductor is costly.
- ✓ Variable inductor is bulky.

### 2.3.2 Maxwell's inductance capacitance bridge

Unknown inductance is measured by comparing it with standard capacitance. In this bridge, balance condition is achieved by varying ' $C_4$ '.

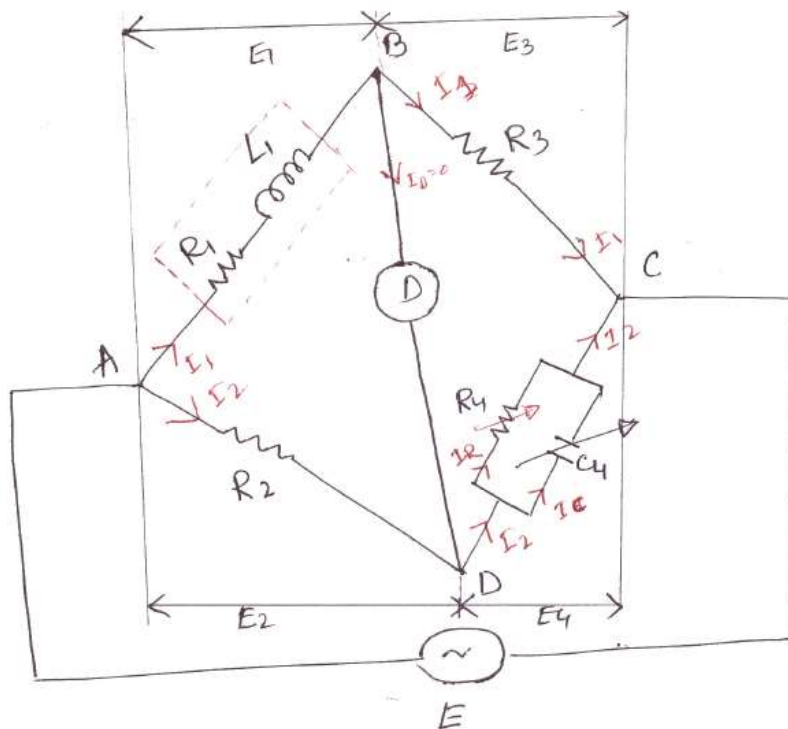


Fig 2.4 Maxwell's inductance capacitance bridge

At balance condition,  $Z_1 Z_4 = Z_3 Z_2$  (2.9)

$$Z_4 = R_4 \parallel \frac{1}{j\omega C_4} = \frac{R_4 \times \frac{1}{j\omega C_4}}{R_4 + \frac{1}{j\omega C_4}}$$

$$Z_4 = \frac{R_4}{j\omega R_4 C_4 + 1} = \frac{R_4}{1 + j\omega R_4 C_4}$$
 (2.10)

∴ Substituting the value of  $Z_4$  from eqn. (2.10) in eqn. (2.9) we get

$$(R_1 + j\omega L_1) \times \frac{R_4}{1 + j\omega R_4 C_4} = R_2 R_3$$

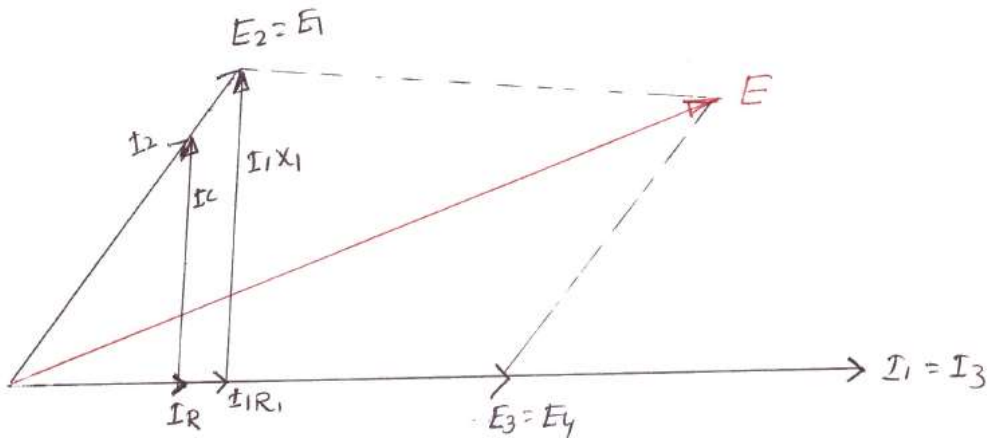


Fig 2.5 Phasor diagram of Maxwell's inductance capacitance bridge

$$(R_1 + j\omega L_1)R_4 = R_2 R_3 (1 + j\omega R_4 C_4)$$

$$R_1 R_4 + j\omega L_1 R_4 = R_2 R_3 + j\omega C_4 R_4 R_2 R_3$$

Comparing real parts,

$$R_1 R_4 = R_2 R_3$$



$$\Rightarrow R_1 = \frac{R_2 R_3}{R_4} \quad (2.11)$$

Comparing imaginary part,

$$\omega L_1 R_4 = \omega C_4 R_4 R_2 R_3$$

$$L_1 = C_4 R_2 R_3 \quad (2.12)$$

Q-factor of choke,

$$Q = \frac{\omega L_1}{R_1} = \omega \times C_4 R_2 R_3 \times \frac{R_4}{R_2 R_3}$$

$$Q = \omega C_4 R_4 \quad (2.13)$$

### Advantages

- ✓ Equation of  $L_1$  and  $R_1$  are simple.
- ✓ They are independent of frequency.
- ✓ They are independent of each other.
- ✓ Standard capacitor is much smaller in size than standard inductor.

### Disadvantages

- ✓ Standard variable capacitance is costly.
- ✓ It can be used for measurements of Q-factor in the ranges of 1 to 10.
- ✓ It cannot be used for measurements of choke with Q-factors more than 10.

We know that  $Q = \omega C_4 R_4$

For measuring chokes with higher value of Q-factor, the value of  $C_4$  and  $R_4$  should be higher. Higher values of standard resistance are very expensive. Therefore this bridge cannot be used for higher value of Q-factor measurements.

### 2.3.3 Hay's bridge

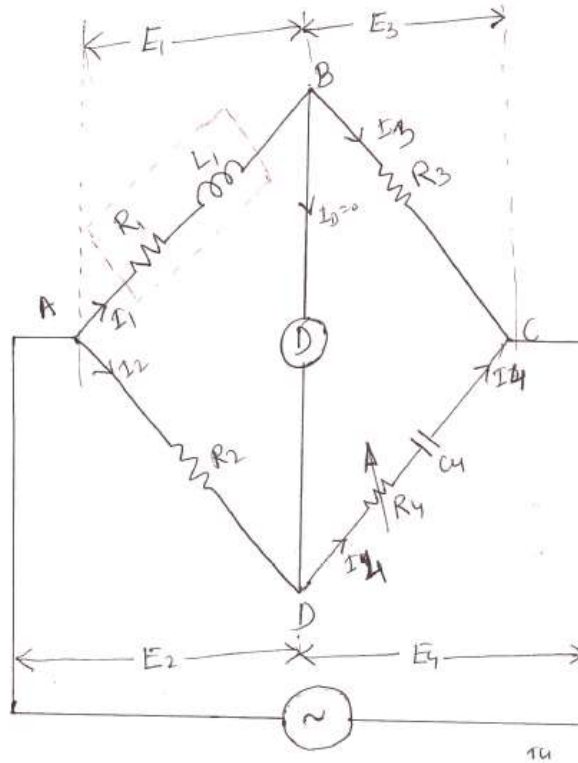


Fig 2.6 Hay's bridge

$$\text{➤ } \dot{E}_1 = I_1 R_1 + jI_1 X_1$$

$$\text{➤ } \dot{E} = \dot{E}_1 + \dot{E}_3$$

$$\text{➤ } \dot{E}_4 = I_4 R_4 + \frac{I_4}{j\omega C_4}$$

$$\text{➤ } \dot{E}_3 = I_3 R_3$$

$$Z_4 = R_4 + \frac{1}{j\omega C_4} = \frac{1 + j\omega R_4 C_4}{j\omega C_4}$$



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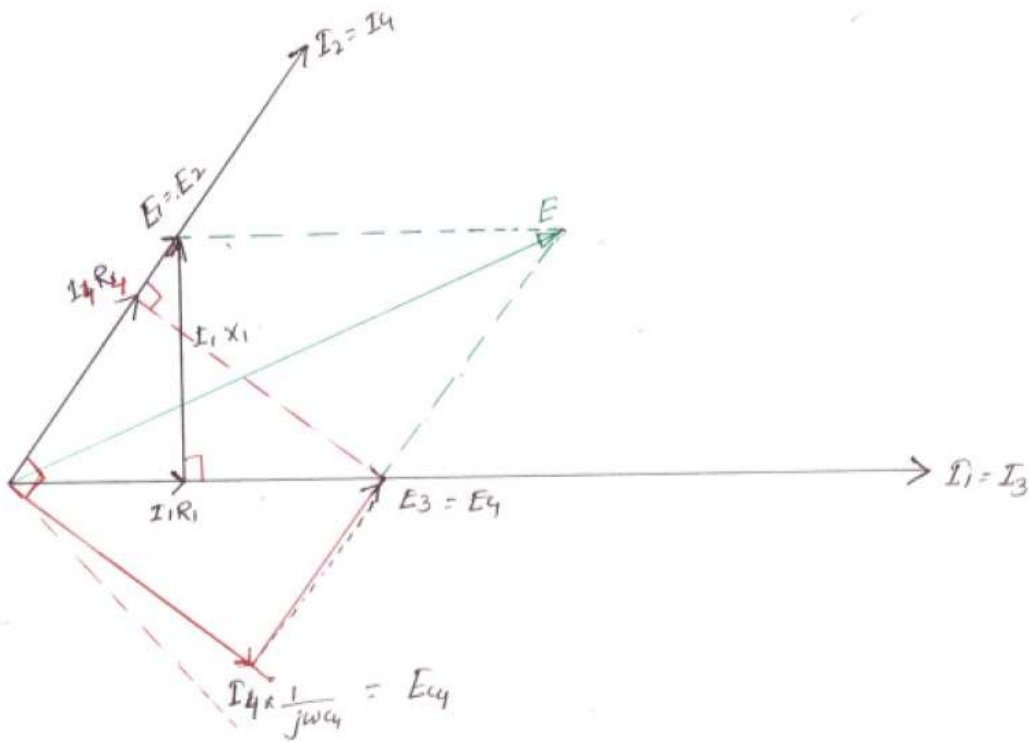


Fig 2.7 Phasor diagram of Hay's bridge

At balance condition,  $Z_1 Z_4 = Z_3 Z_2$

$$(R_1 + j\omega L_1) \left( \frac{1 + j\omega R_4 C_4}{j\omega C_4} \right) = R_2 R_3$$

$$(R_1 + j\omega L_1)(1 + j\omega R_4 C_4) = j\omega R_2 C_4 R_3$$

$$R_1 + j\omega C_4 R_4 R_1 + j\omega L_1 + j^2 \omega^2 L_1 C_4 R_4 = j\omega C_4 R_2 R_3$$

$$(R_1 - \omega^2 L_1 C_4 R_4) + j(\omega C_4 R_4 R_1 + \omega L_1) = j\omega C_4 R_2 R_3$$

Comparing the real term,

$$R_1 - \omega^2 L_1 C_4 R_4 = 0$$

$$R_1 = \omega^2 L_1 C_4 R_4 \tag{2.14}$$





Comparing the imaginary terms,

$$wC_4R_4R_1 + wL_1 = wC_4R_2R_3$$

$$C_4R_4R_1 + L_1 = C_4R_2R_3$$

$$L_1 = C_4R_2R_3 - C_4R_4R_1 \quad (2.15)$$

Substituting the value of  $R_1$  from eqn. 2.14 into eqn. 2.15, we have,

$$L_1 = C_4R_2R_3 - C_4R_4 \times w^2L_1C_4R_4$$

$$L_1 = C_4R_2R_3 - w^2L_1C_4^2R_4^2$$

$$L_1(1 + w^2L_1C_4^2R_4^2) = C_4R_2R_3$$

$$L_1 = \frac{C_4R_2R_3}{1 + w^2L_1C_4^2R_4^2} \quad (2.16)$$

Substituting the value of  $L_1$  in eqn. 2.14, we have

$$R_1 = \frac{w^2C_4^2R_2R_3R_4}{1 + w^2C_4^2R_4^2} \quad (2.17)$$

$$Q = \frac{wL_1}{R_1} = \frac{w \times C_4R_2R_3}{1 + w^2C_4^2R_4^2} \times \frac{1 + w^2C_4^2R_4^2}{w^2C_4^2R_4R_2R_3}$$

$$Q = \frac{1}{wC_4R_4} \quad (2.18)$$

### Advantages

- ✓ Fixed capacitor is cheaper than variable capacitor.
- ✓ This bridge is best suitable for measuring high value of Q-factor.

### Disadvantages

- ✓ Equations of  $L_1$  and  $R_1$  are complicated.
- ✓ Measurements of  $R_1$  and  $L_1$  require the value of frequency.
- ✓ This bridge cannot be used for measuring low Q-factor.

### 2.3.4 Owen's bridge

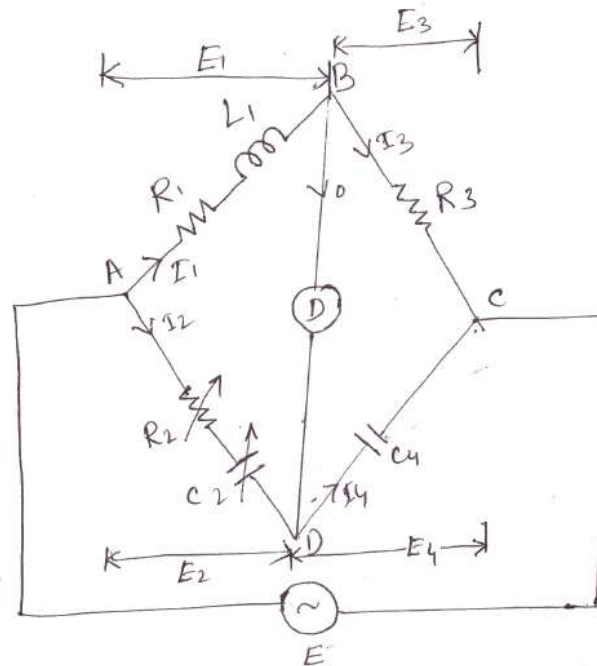


Fig 2.8 Owen's bridge

- $E_1 = I_1 R_1 + jI_1 X_1$
- $I_4$  leads  $E_4$  by  $90^\circ$

- $\dot{E} = \dot{E}_1 + \dot{E}_3$
- $\dot{E}_2 = I_2 R_2 + \frac{I_2}{j\omega C_2}$

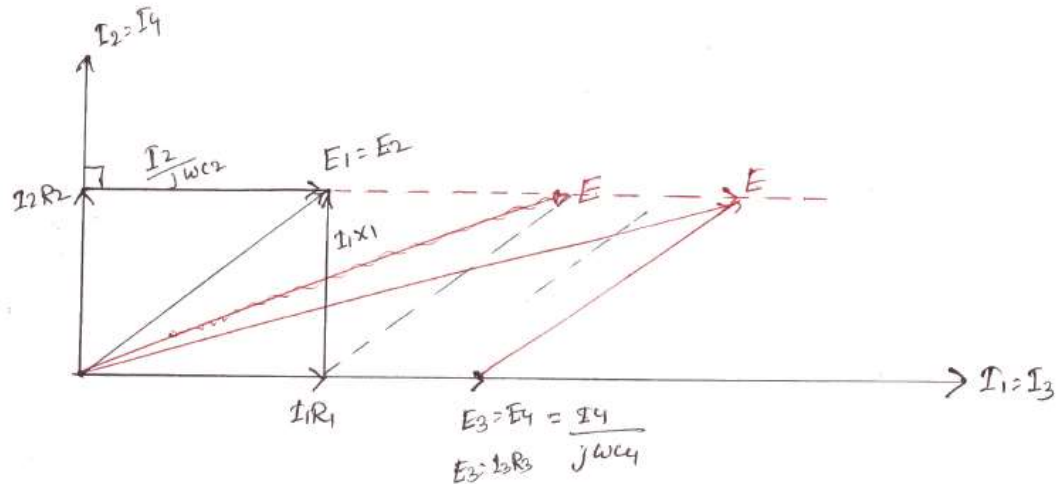


Fig 2.9 Phasor diagram of Owen's bridge

**Balance condition,**  $\dot{Z}_1 \dot{Z}_4 = \dot{Z}_2 \dot{Z}_3$

$$Z_2 = R_2 + \frac{1}{j\omega C_2} = \frac{j\omega C_2 R_2 + 1}{j\omega C_2}$$

$$\therefore (R_1 + j\omega L_1) \times \frac{1}{j\omega C_4} = \frac{(1 + j\omega R_2 C_2) \times R_3}{j\omega C_2}$$

$$C_2 (R_1 + j\omega L_1) = R_3 C_4 (1 + j\omega R_2 C_2)$$

$$R_1 C_2 + j\omega L_1 C_2 = R_3 C_4 + j\omega R_2 C_2 R_3 C_4$$

Comparing real terms,

$$R_1 C_2 = R_3 C_4$$



$$R_1 = \frac{R_3 C_4}{C_2}$$

Comparing imaginary terms,

$$wL_1 C_2 = wR_2 C_2 R_3 C_4$$

$$L_1 = R_2 R_3 C_4$$

$$Q\text{-factor} = \frac{WL_1}{R_1} = \frac{wR_2 R_3 C_4 C_2}{R_3 C_4}$$

$$Q = wR_2 C_2$$

### Advantages

- ✓ Expression for  $R_1$  and  $L_1$  are simple.
- ✓  $R_1$  and  $L_1$  are independent of Frequency.

### Disadvantages

- ✓ The Circuits used two capacitors.
- ✓ Variable capacitor is costly.
- ✓ Q-factor range is restricted.



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### 2.3.5 Anderson's bridge

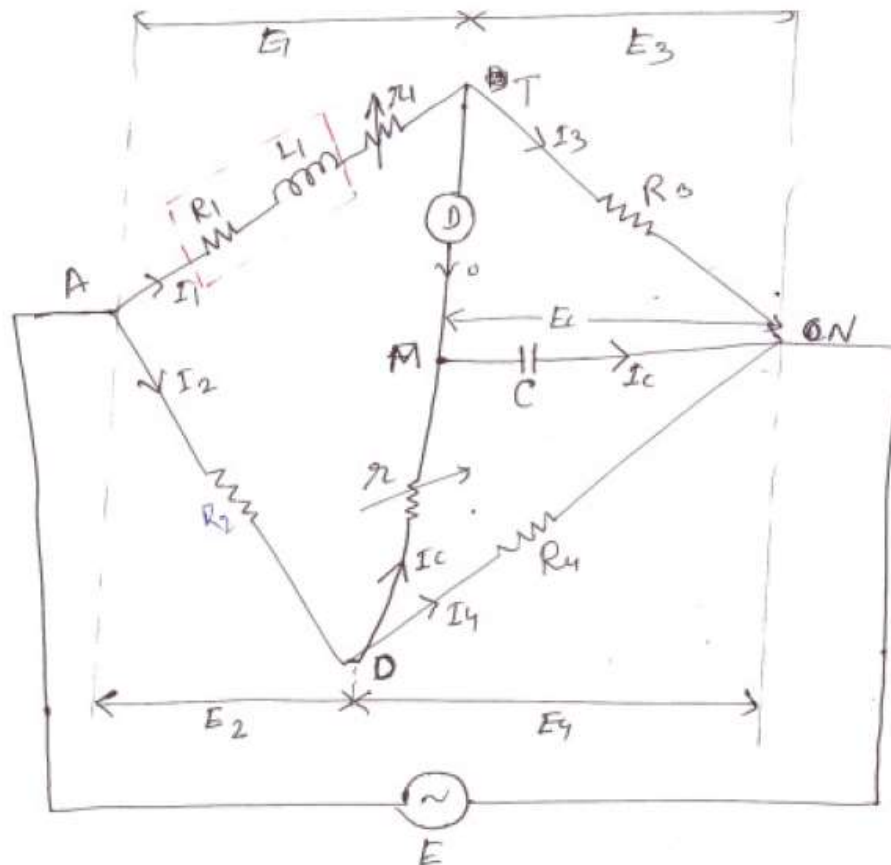


Fig 2.10 Anderson's bridge

- $\dot{E}_1 = I_1(R_1 + r_1) + jI_1X_1$
- $E_3 = E_C$
- $\dot{E}_4 = I_C r + E_C$
- $I_2 = I_4 + I_C$
- $\bar{E}_2 + \bar{E}_4 = \bar{E}$
- $\bar{E}_1 + \bar{E}_3 = \bar{E}$

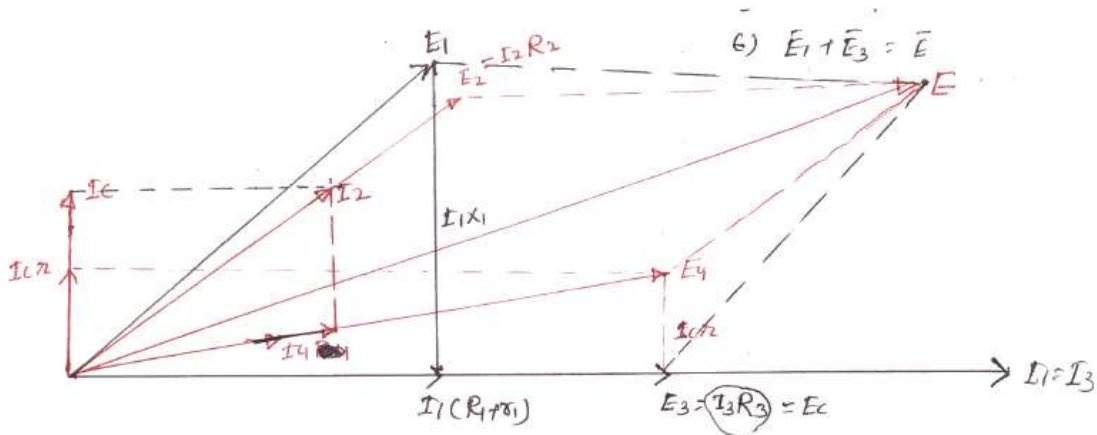


Fig 2.11 Phasor diagram of Anderson's bridge

**Step-1** Take  $I_1$  as references vector .Draw  $I_1R_1^1$  in phase with  $I_1$

$$R_1^1 = (R_1 + r_1) , I_1X_1 \text{ is } \perp_r \text{ to } I_1R_1^1$$

$$E_1 = I_1R_1^1 + jI_1X_1$$

**Step-2**  $I_1 = I_3$  ,  $E_3$  is in phase with  $I_3$  , From the circuit ,

$$E_3 = E_C , I_C \text{ leads } E_C \text{ by } 90^\circ$$

**Step-3**  $E_4 = I_Cr + E_C$

**Step-4** Draw  $I_4$  in phase with  $E_4$  , By KCL ,  $I_2 = I_4 + I_C$

**Step-5** Draw  $E_2$  in phase with  $I_2$

**Step-6** By KVL ,  $\bar{E}_1 + \bar{E}_3 = \bar{E}$  or  $\bar{E}_2 + \bar{E}_4 = \bar{E}$

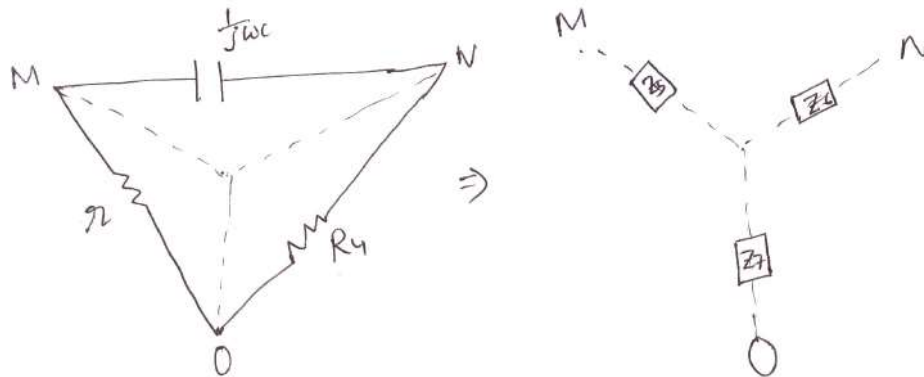


Fig 2.12 Equivalent delta to star conversion for the loop MON

$$Z_7 = \frac{R_4 \times r}{R_4 + r + \frac{1}{j\omega C}} = \frac{j\omega C R_4 r}{1 + j\omega C(R_4 + r)}$$

$$Z_6 = \frac{R_4 \times \frac{1}{j\omega C}}{R_4 + r + \frac{1}{j\omega C}} = \frac{R_4}{1 + j\omega C(R_4 + r)}$$

$$(R_1^1 + j\omega L_1) \times \frac{R_4}{1 + j\omega C(R_4 + r)} = R_3 \left( R_2 + \frac{j\omega C R_4 r}{1 + j\omega C(R_4 + r)} \right)$$

$$\Rightarrow \frac{(R_1^1 + j\omega L_1) R_4}{1 + j\omega C(R_4 + r)} = R_3 \left[ \frac{R_2(1 + j\omega C(R_4 + r)) + j\omega C r R_4}{1 + j\omega C(R_4 + r)} \right]$$

$$\Rightarrow R_1^1 R_4 + j\omega L_1 R_4 = R_2 R_3 + j\omega C r R_2 R_3 (r + R_4) + j\omega C r R_4 R_3$$





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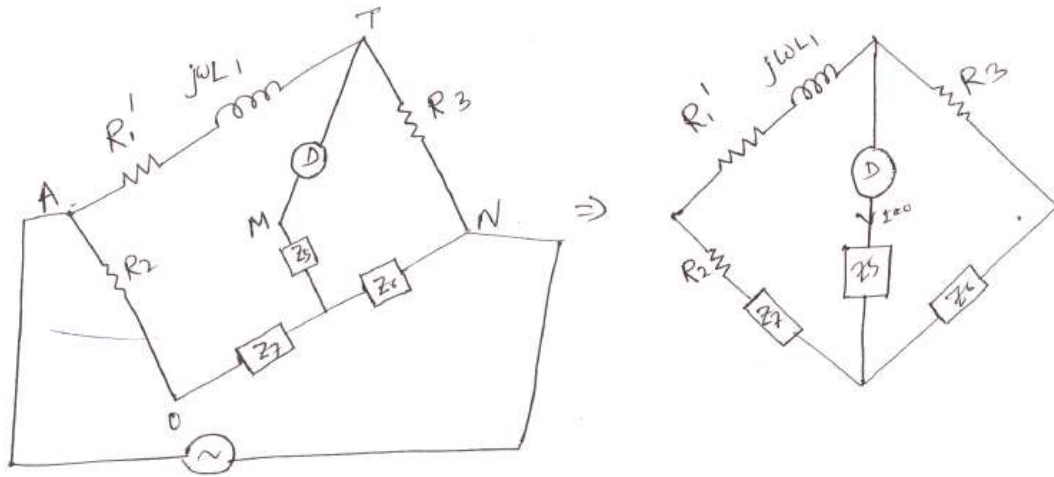


Fig 2.13 Simplified diagram of Anderson's bridge

Comparing real term,

$$R_1^1 R_4 = R_2 R_3$$

$$(R_1 + r_1) R_4 = R_2 R_3$$

$$R_1 = \frac{R_2 R_3}{R_4} - r_1$$

Comparing the imaginary term,

$$wL_1 R_4 = wCR_2 R_3 (r + R_4) + wcrR_3 R_4$$

$$L_1 = \frac{R_2 R_3 C}{R_4} (r + R_4) + R_3 r C$$

$$L_1 = R_3 C \left[ \frac{R_2}{R_4} (r + R_4) + r \right]$$

### Advantages

- ✓ Variable capacitor is not required.
- ✓ Inductance can be measured accurately.
- ✓  $R_1$  and  $L_1$  are independent of frequency.
- ✓ Accuracy is better than other bridges.

### Disadvantages

- ✓ Expression for  $R_1$  and  $L_1$  are complicated.
- ✓ This is not in the standard form A.C. bridge.

## 2.4 Measurement of capacitance and loss angle. (Dissipation factor)

### 2.4.1 Dissipation factors (D)

A practical capacitor is represented as the series combination of small resistance and ideal capacitance.

From the vector diagram, it can be seen that the angle between voltage and current is slightly less than  $90^\circ$ . The angle ' $\delta$ ' is called loss angle.

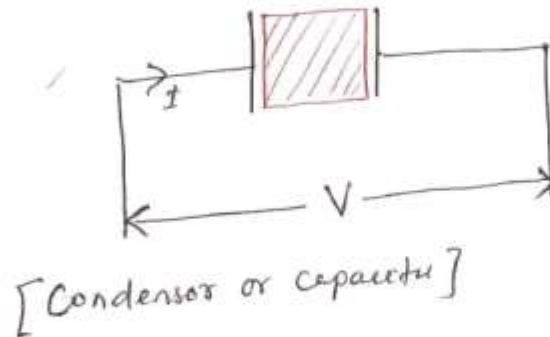


Fig 2.14 Condensor or capacitor

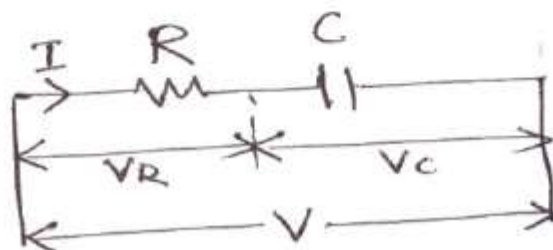


Fig 2.15 Representation of a practical capacitor



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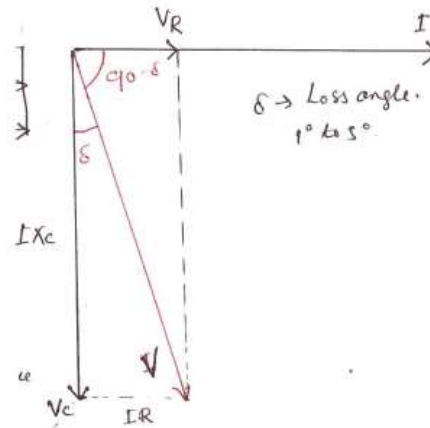


Fig 2.16 Vector diagram for a practical capacitor

A dissipation factor is defined as 'tan  $\delta$ '.

$$\therefore \tan \delta = \frac{IR}{IX_C} = \frac{R}{X_C} = \omega CR$$

$$D = \omega CR$$

$$D = \frac{1}{Q}$$

$$D = \tan \delta = \frac{\sin \delta}{\cos \delta} \cong \frac{\delta}{1} \quad \text{For small value of '}\delta\text{' in radians}$$

$$D \cong \delta \cong \text{Loss Angle} \quad (\delta \text{ must be in radian})$$

### 2.4.2 Desauty's Bridge

$C_1$  = Unknown capacitance

At balance condition,

$$\frac{1}{j\omega C_1} \times R_4 = \frac{1}{j\omega C_2} \times R_3$$

$$\frac{R_4}{C_1} = \frac{R_3}{C_2}$$

$$\Rightarrow C_1 = \frac{R_4 C_2}{R_3}$$

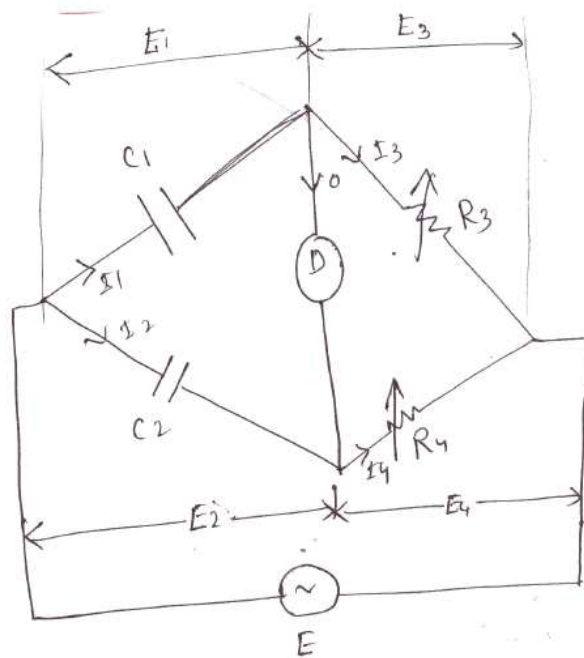


Fig 2.17 Desauty's bridge

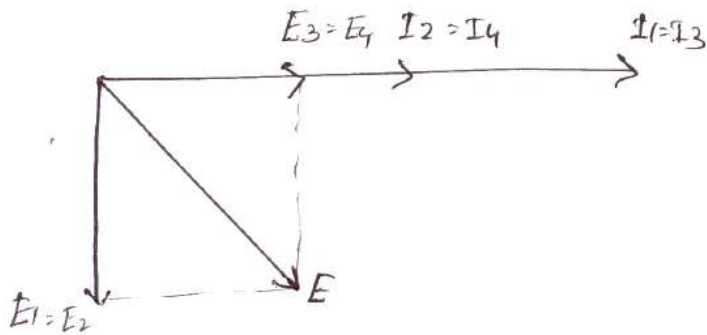


Fig 2.18 Phasor diagram of Desauty's bridge

2.4.3 Modified desauty's bridge

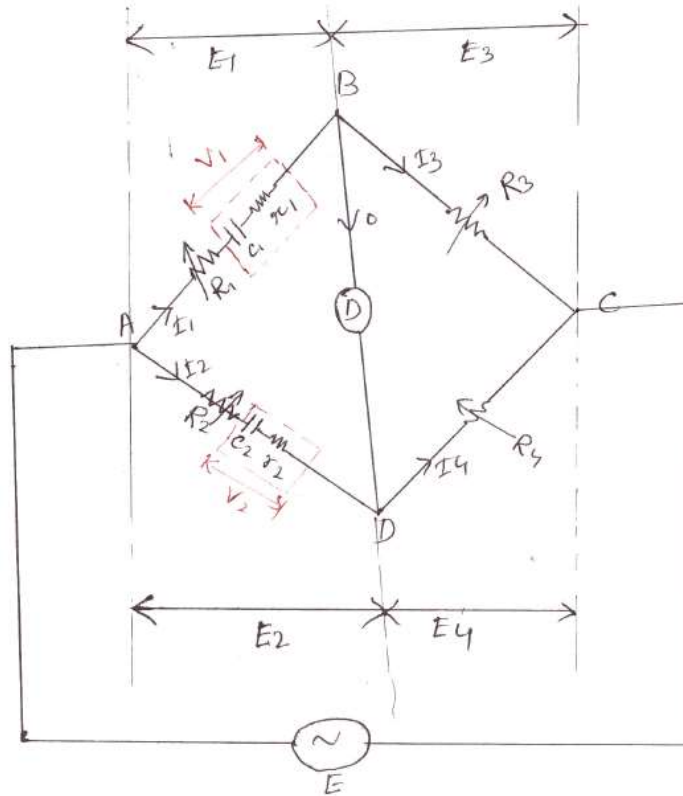


Fig 2.19 Modified Desauty's bridge

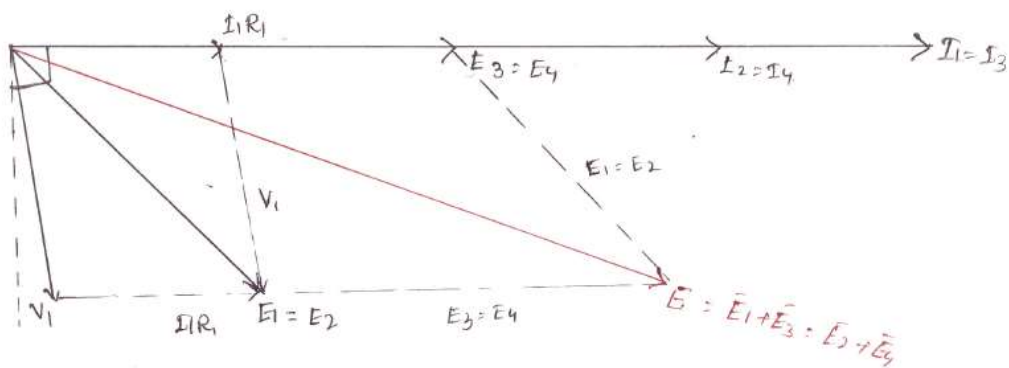


Fig 2.20 Phasor diagram of Modified Desauty's bridge

$$R_1^1 = (R_1 + r_1)$$

$$R_2^1 = (R_2 + r_2)$$

$$\text{At balance condition, } (R_1^1 + \frac{1}{j\omega C_1})R_4 = R_3(R_2^1 + \frac{1}{j\omega C_2})$$

$$R_1^1 R_4 + \frac{R_4}{j\omega C_1} = R_3 R_2^1 + \frac{R_3}{j\omega C_2}$$

$$\text{Comparing the real term, } R_1^1 R_4 = R_3 R_2^1$$

$$R_1^1 = \frac{R_3 R_2^1}{R_4}$$

$$R + r_1 = \frac{(R_2 + r_2) R_3}{R_4}$$

Comparing imaginary term,

$$\frac{R_4}{\omega C_1} = \frac{R_3}{\omega C_2}$$

$$C_1 = \frac{R_4 C_2}{R_3}$$

Dissipation factor  $D = \omega C_1 r_1$

#### Advantages

- ✓  $r_1$  and  $c_1$  are independent of frequency.
- ✓ They are independent of each other.
- ✓ Source need not be pure sine wave.

#### 2.4.4 Schering bridge

$$E_1 = I_1 r_1 - j I_1 X_4$$

$C_2 = C_4 =$  Standard capacitor (Internal resistance=0)

$C_4 =$  Variable capacitance.

$C_1 =$  Unknown capacitance.

$r_1 =$  Unknown series equivalent resistance of the capacitor.



$R_3=R_4=$  Known resistor.

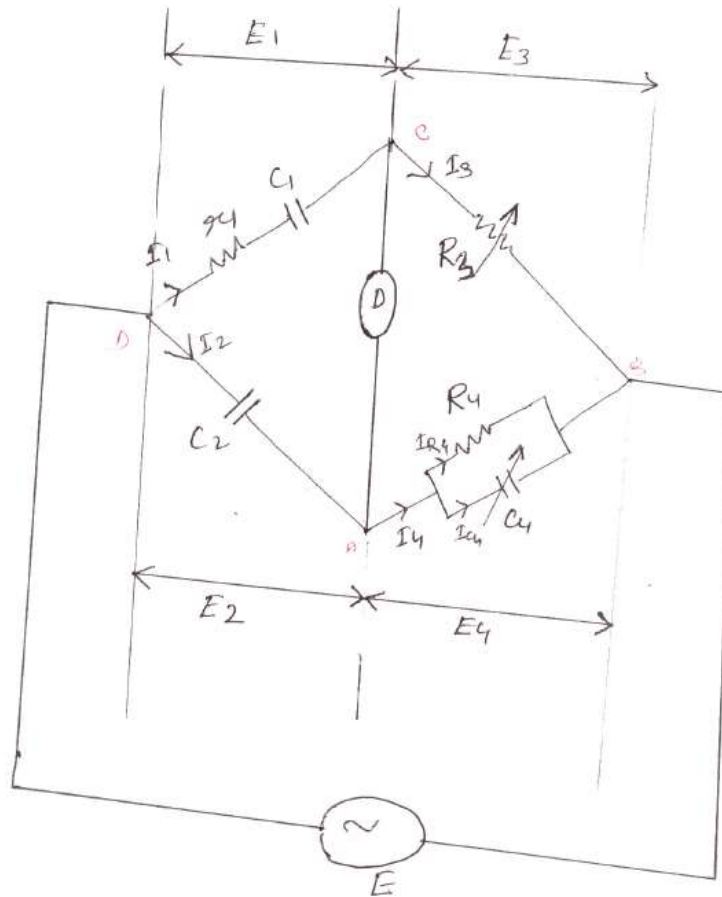


Fig 2.21 Schering bridge

$$Z_1 = r_1 + \frac{1}{j\omega C_1} = \frac{j\omega C_1 r_1 + 1}{j\omega C_1}$$

$$Z_4 = \frac{R_4 \times \frac{1}{j\omega C_4}}{R_4 + \frac{1}{j\omega C_4}} = \frac{R_4}{1 + j\omega C_4 R_4}$$

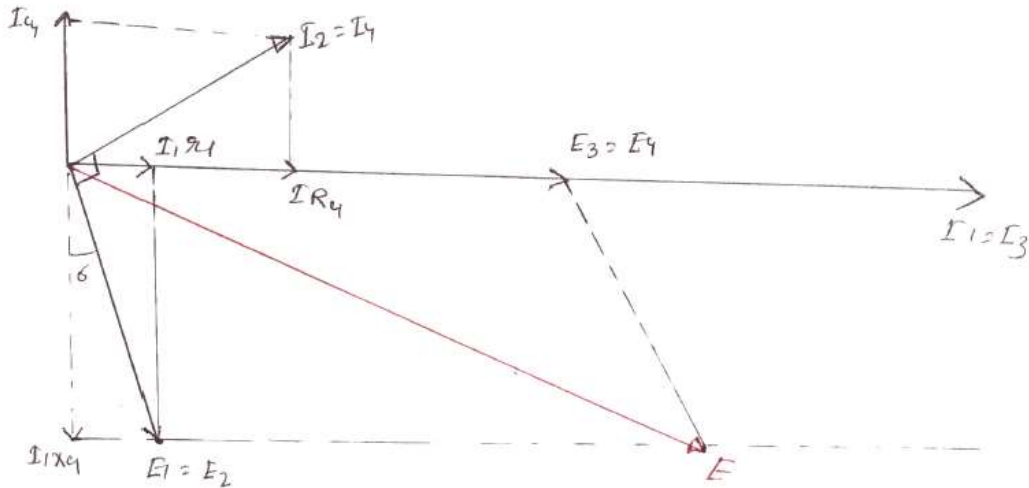


Fig 2.22 Phasor diagram of Schering bridge

At balance condition,  $\dot{Z}_1 \dot{Z}_4 = \dot{Z}_2 \dot{Z}_3$

$$\frac{1 + j\omega C_1 r_1}{j\omega C_1} \times \frac{R_4}{1 + j\omega C_4 R_4} = \frac{R_3}{j\omega C_2}$$

$$(1 + j\omega C_1 r_1) R_4 C_2 = R_3 C_1 (1 + j\omega C_4 R_4)$$

$$R_2 C_2 + j\omega C_1 r_1 R_4 C_2 = R_3 C_1 + j\omega C_4 R_4 R_3 C_1$$

Comparing the real part,

$$\therefore C_1 = \frac{R_4 C_2}{R_3}$$

Comparing the imaginary part,

$$\omega C_1 r_1 R_4 C_2 = \omega C_4 R_3 R_4 C_1$$

$$r_1 = \frac{C_4 R_3}{C_2}$$

Dissipation factor of capacitor,



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$$D = wC_1r_1 = w \times \frac{R_4C_2}{R_3} \times \frac{C_4R_3}{C_2}$$

$$\therefore D = wC_4R_4$$

### Advantages

- ✓ In this type of bridge, the value of capacitance can be measured accurately.
- ✓ It can measure capacitance value over a wide range.
- ✓ It can measure dissipation factor accurately.

### Disadvantages

- ✓ It requires two capacitors.
- ✓ Variable standard capacitor is costly.

## 2.5 Measurements of frequency

### 2.5.1 Wein's bridge

Wein's bridge is popularly used for measurements of frequency of frequency. In this bridge, the value of all parameters are known. The source whose frequency has to measure is connected as shown in the figure.

$$Z_1 = r_1 + \frac{1}{j\omega C_1} = \frac{j\omega C_1 r_1 + 1}{j\omega C_1}$$

$$Z_2 = \frac{R_2}{1 + j\omega C_2 R_2}$$

At balance condition,  $\dot{Z}_1 \dot{Z}_4 = \dot{Z}_2 \dot{Z}_3$

$$\frac{j\omega C_1 r_1 + 1}{j\omega C_1} \times R_4 = \frac{R_2}{1 + j\omega C_2 R_2} \times R_3$$

$$(1 + j\omega C_1 r_1)(1 + j\omega C_2 R_2)R_4 = R_2 R_3 \times j\omega C_1$$

$$\left[ 1 + j\omega C_2 R_2 + j\omega C_1 r_1 - \omega^2 C_1 C_2 r_1 R_2 \right] = j\omega C_1 \frac{R_2 R_3}{R_4}$$

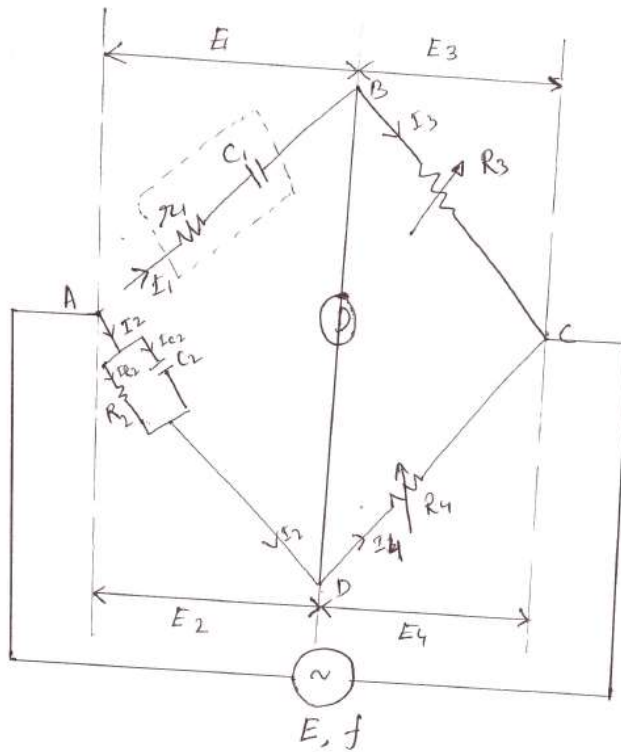


Fig 2.23 Wein's bridge

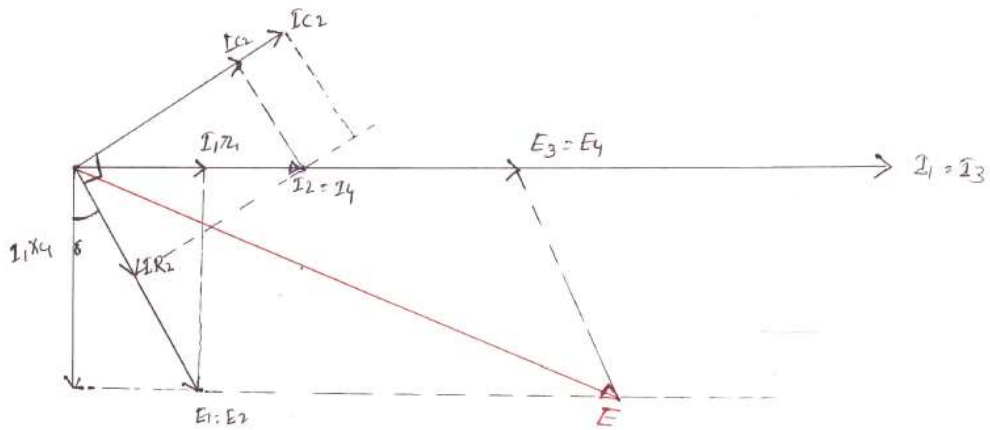


Fig 2.24 Phasor diagram of Wein's bridge



Comparing real term,

$$1 - w^2 C_1 C_2 r_1 R_2 = 0$$

$$w^2 C_1 C_2 r_1 R_2 = 1$$

$$w^2 = \frac{1}{C_1 C_2 r_1 R_2}$$

$$w = \frac{1}{\sqrt{C_1 C_2 r_1 R_2}}, \quad f = \frac{1}{2\pi \sqrt{C_1 C_2 r_1 R_2}}$$

**NOTE**

The above bridge can be used for measurements of capacitance. In such case,  $r_1$  and  $C_1$  are unknown and frequency is known. By equating real terms, we will get  $R_1$  and  $C_1$ . Similarly by equating imaginary term, we will get another equation in terms of  $r_1$  and  $C_1$ . It is only used for measurements of Audio frequency.

A.F=20 HZ to 20 KHZ

R.F=>> 20 KHZ

Comparing imaginary term,

$$w C_2 R_2 + w C_1 r_1 = w C_1 \frac{R_2 R_3}{R_4}$$

$$C_2 R_2 + C_1 r_1 = \frac{C_1 R_2 R_3}{R_4} \dots\dots\dots(2.19)$$

$$C_1 = \frac{1}{w^2 C_2 r_1 R_2}$$

Substituting in eqn. (2.19), we have

$$C_2 R_2 + \frac{r_1}{w^2 C_2 r_1 R_2} = \frac{R_2 R_3}{R_4} C_1$$

Multiplying  $\frac{R_4}{R_2 R_3}$  in both sides, we have

$$C_2 R_2 \times \frac{R_4}{R_2 R_3} + \frac{1}{w^2 C_2 R_2} \times \frac{R_4}{R_2 R_3} = C_1$$

$$C_1 = \frac{C_2 R_4}{R_3} + \frac{R_4}{w^2 C_2 R_2^2 R_3}$$

$$w^2 C_1 r_1 C_2 R_2 = 1$$

$$r_1 = \frac{1}{w^2 C_2 R_2 C_1} = \frac{1}{w^2 C_2 R_2 \left[ \frac{C_2 R_4}{R_3} + \frac{R_4}{w^2 C_2 R_2^2 R_3} \right]}$$

$$= \frac{1}{\left[ \frac{w^2 C_2^2 R_2 R_4}{R_3} + \frac{R_4}{R_2 R_3} \right]}$$

$$\therefore r_1 = \frac{1}{\frac{R_3}{R_4} \left[ w^2 C_2^2 R_2 + \frac{1}{R_2} \right]}$$

$$\therefore r_1 = \frac{R_3}{R_4} \left[ \frac{1}{(w^2 C_2^2 R_2 + \frac{1}{R_2})} \right]$$

### 2.5.2 High Voltage Schering Bridge

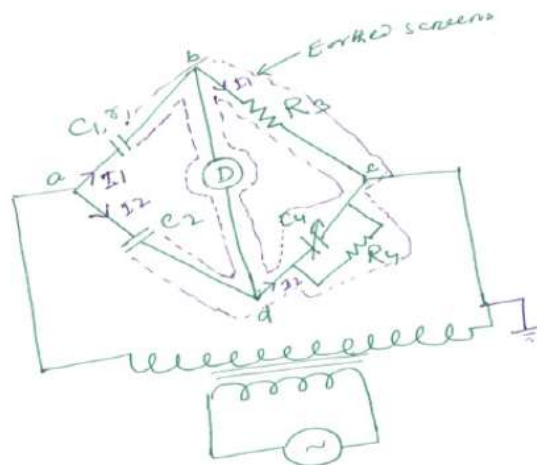


Fig 2.25 High Voltage Schering bridge

(1) The high voltage supply is obtained from a transformer usually at 50 HZ.

### 2.6 Wagner earthing device:

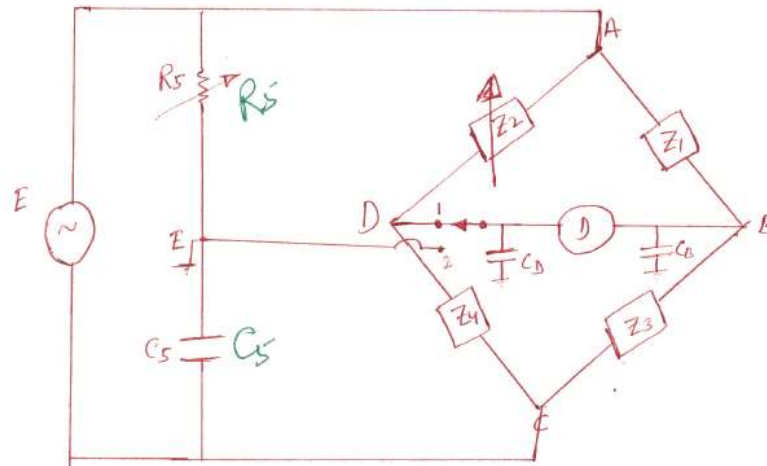


Fig 2.26 Wagner Earthing device

Wagner earthing consists of 'R' and 'C' in series. The stray capacitance at node 'B' and 'D' are  $C_B$ ,  $C_D$  respectively. These Stray capacitances produced error in the measurements of 'L' and 'C'. These error will predominant at high frequency. The error due to this capacitance can be eliminated using wagner earthing arm.

Close the change over switch to the position (1) and obtained balanced. Now change the switch to position (2) and obtained balance. This process has to repeat until balance is achieved in both the position. In this condition the potential difference across each capacitor is zero. Current drawn by this is zero. Therefore they do not have any effect on the measurements.

#### What are the sources of error in the bridge measurements?

- ✓ Error due to stray capacitance and inductance.
- ✓ Due to external field.
- ✓ Leakage error: poor insulation between various parts of bridge can produced this error.
- ✓ Eddy current error.
- ✓ Frequency error.





- ✓ Waveform error (due to harmonics)
- ✓ Residual error: small inductance and small capacitance of the resistor produce this error.

### Precaution

- ✓ The load inductance is eliminated by twisting the connecting the connecting lead.
- ✓ In the case of capacitive bridge, the connecting lead are kept apart. ( $\because C = \frac{A\epsilon_0\epsilon_r}{d}$ )
- ✓ In the case of inductive bridge, the various arm are magnetically screen.
- ✓ In the case of capacitive bridge, the various arm are electro statically screen to reduced the stray capacitance between various arm.
- ✓ To avoid the problem of spike, an inter bridge transformer is used in between the source and bridge.
- ✓ The stray capacitance between the ends of detector to the ground, cause difficulty in balancing as well as error in measurements. To avoid this problem, we use wagner earthing device.

### 2.7 Ballastic galvanometer

This is a sophisticated instrument. This works on the principle of PMMC meter. The only difference is the type of suspension is used for this meter. Lamp and glass scale method is used to obtain the deflection. A small mirror is attached to the moving system. Phosphorous bronze wire is used for suspension.

When the D.C. voltage is applied to the terminals of moving coil, current flows through it. When a current carrying coil kept in the magnetic field, produced by permanent magnet, it experiences a force. The coil deflects and mirror deflects. The light spot on the glass scale also move. This deflection is proportional to the current through the coil.

$$i = \frac{Q}{t}, Q = it = \int idt$$

$$\theta \propto Q, \text{ deflection} \propto \text{Charge}$$



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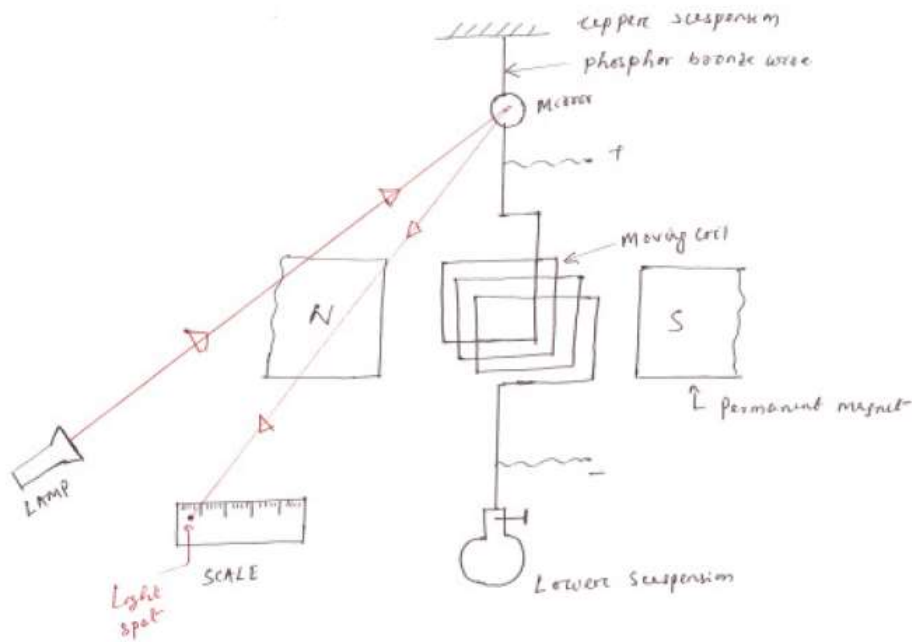


Fig 2.27 Ballistic galvanometer

### 2.8 Measurements of flux and flux density (Method of reversal)

D.C. voltage is applied to the electromagnet through a variable resistance  $R_1$  and a reversing switch. The voltage applied to the toroid can be reversed by changing the switch from position 2 to position '1'. Let the switch be in position '2' initially. A constant current flows through the toroid and a constant flux is established in the core of the magnet.

A search coil of few turns is provided on the toroid. The B.G. is connected to the search coil through a current limiting resistance. When it is required to measure the flux, the switch is changed from position '2' to position '1'. Hence the flux reduced to zero and it starts increasing in the reverse direction. The flux goes from  $+\phi$  to  $-\phi$ , in time 't' second. An emf is induced in the search coil, since the flux changes with time. This emf circulates a current through  $R_2$  and B.G. The meter deflects. The switch is normally closed. It is opened when it is required to take the reading.

### 2.8.1 Plotting the BH curve

The curve drawn with the current on the X-axis and the flux on the Y-axis, is called magnetization characteristics. The shape of B-H curve is similar to shape of magnetization characteristics. The residual magnetism present in the specimen can be removed as follows.

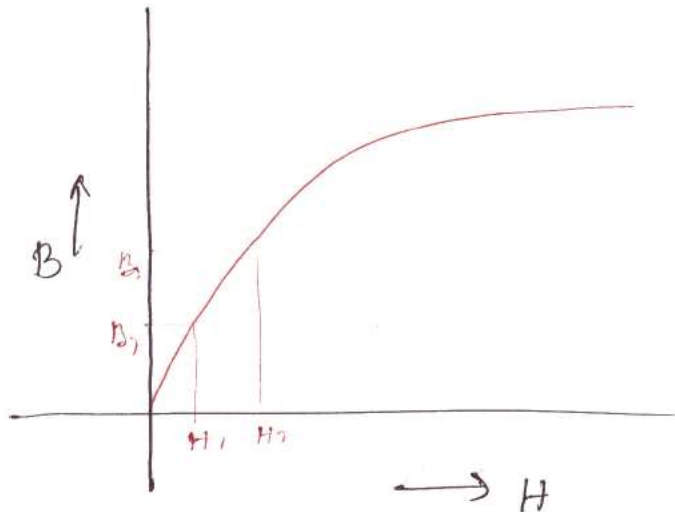


Fig 2.28 BH curve

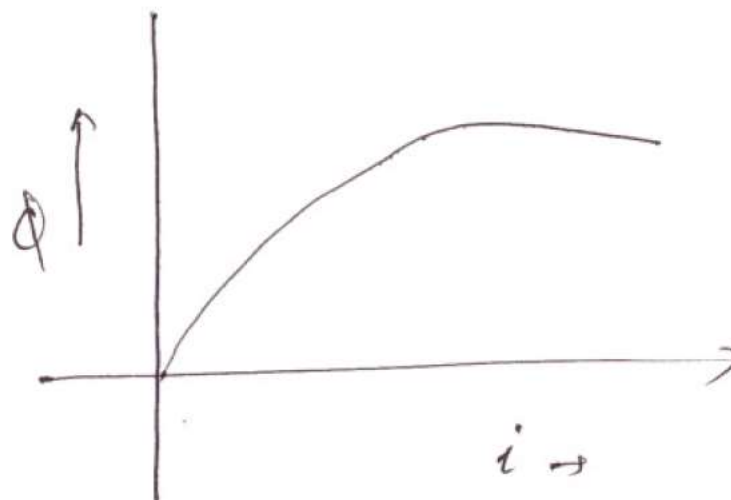


Fig 2.29 Magnetization characteristics



Close the switch 'S<sub>2</sub>' to protect the galvanometer, from high current. Change the switch S<sub>1</sub> from position '1' to '2' and vice versa for several times.

To start with the resistance 'R<sub>1</sub>' is kept at maximum resistance position. For a particular value of current, the deflection of B.G. is noted. This process is repeated for various value of current. For each deflection flux can be calculated. ( $B = \frac{\phi}{A}$ )

Magnetic field intensity value for various current can be calculated.().The B-H curve can be plotted by using the value of 'B' and 'H'.

### 2.8.2 Measurements of iron loss:

Let R<sub>p</sub>= pressure coil resistance

R<sub>S</sub> = resistance of coil S<sub>1</sub>

E= voltage reading= Voltage induced in S<sub>2</sub>

I= current in the pressure coil

V<sub>p</sub>= Voltage applied to wattmeter pressure coil.

W= reading of wattmeter corresponding voltage V

W<sub>1</sub>= reading of wattmeter corresponding voltage E

$$\begin{array}{l} W \rightarrow V \\ W_1 \rightarrow E_p \end{array} \quad \frac{W_1}{W} = \frac{E}{V} \Rightarrow W_1 = \frac{E \times W}{V}$$

W<sub>1</sub>=Total loss=Iron loss+ Copper loss.

The above circuit is similar to no load test of transformer.

In the case of no load test the reading of wattmeter is approximately equal to iron loss. Iron loss depends on the emf induced in the winding. Science emf is directly proportional to flux. The voltage applied to the pressure coil is V. The corresponding of wattmeter is 'W'. The iron loss corresponding E is  $E = \frac{WE}{V}$ . The reading of the wattmeter includes the losses in the pressure coil and copper loss of the winding S<sub>1</sub>. These losses have to be subtracted to get the actual iron loss.

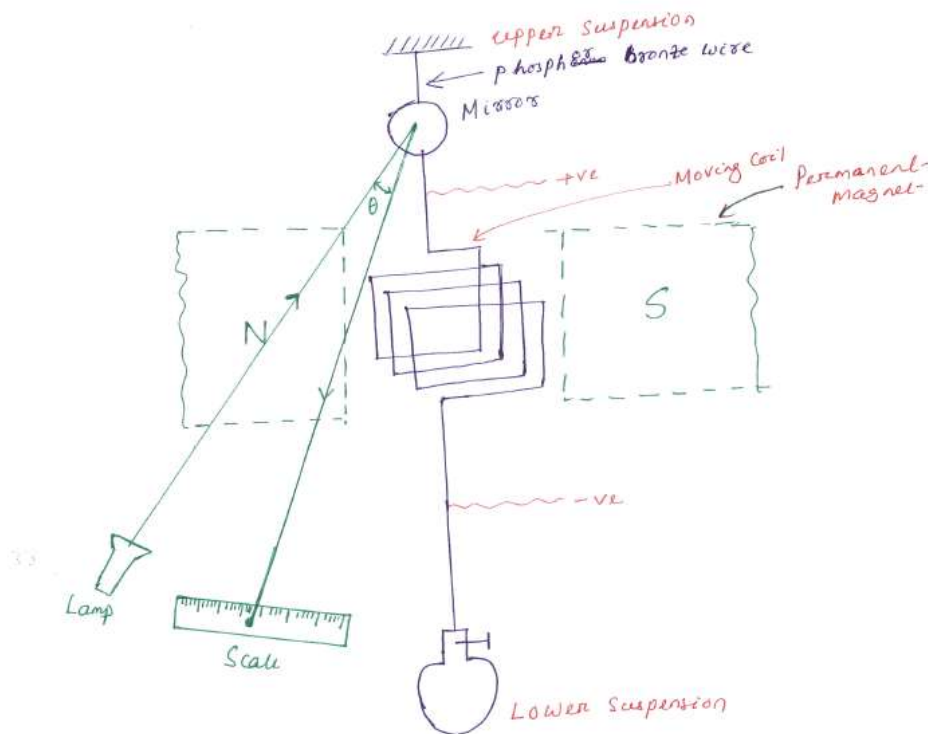
## 2.9 Galvanometers

D-Arsonval Galvanometer

Vibration Galvanometer

Ballistic C

### 2.9.1 D-aronval galvanometer (d.c. galvanometer)



**Fig 2.30** D-Arsonval Galvanometer

Galvanometer is a special type of ammeter used for measuring  $\mu A$  or mA. This is a sophisticated instruments. This works on the principle of PMMC meter. The only difference is the type of suspension used for this meter. It uses a sophisticated suspension called taut suspension, so that moving system has negligible weight.

Lamp and glass scale method is used to obtain the deflection. A small mirror is attached to the moving system. Phosphors bronze is used for suspension.



When D.C. voltage is applied to the terminal of moving coil, current flows through it. When current carrying coil is kept in the magnetic field produced by P.M. , it experiences a force. The light spot on the glass scale also move. This deflection is proportional to the current through the coil. This instrument can be used only with D.C. like PMMC meter.

The deflecting Torque,

$$T_D = BINA$$

$$T_D = GI, \quad \text{Where } G = BAN$$

$$T_C = K_S \theta = S \theta$$

$$\text{At balance, } T_C = T_D \Rightarrow S \theta = GI$$

$$\therefore \theta = \frac{GI}{S}$$

Where  $G$  = Displacements constant of Galvanometer

$S$  = Spring constant

### **2.9.2 Vibration Galvanometer (A.C. Galvanometer)**

The construction of this galvanometer is similar to the PMMC instrument except for the moving system. The moving coil is suspended using two ivory bridge pieces. The tension of the system can be varied by rotating the screw provided at the top suspension. The natural frequency can be varied by varying the tension wire of the screw or varying the distance between ivory bridge piece.

When A.C. current is passed through coil an alternating torque or vibration is produced. This vibration is maximum if the natural frequency of moving system coincide with supply frequency. Vibration is maximum, science resonance takes place. When the coil is vibrating , the mirror oscillates and the dot moves back and front. This appears as a line on the glass scale. Vibration galvanometer is used for null deflection of a dot appears on the scale. If the bridge is unbalanced, a line appears on the scale



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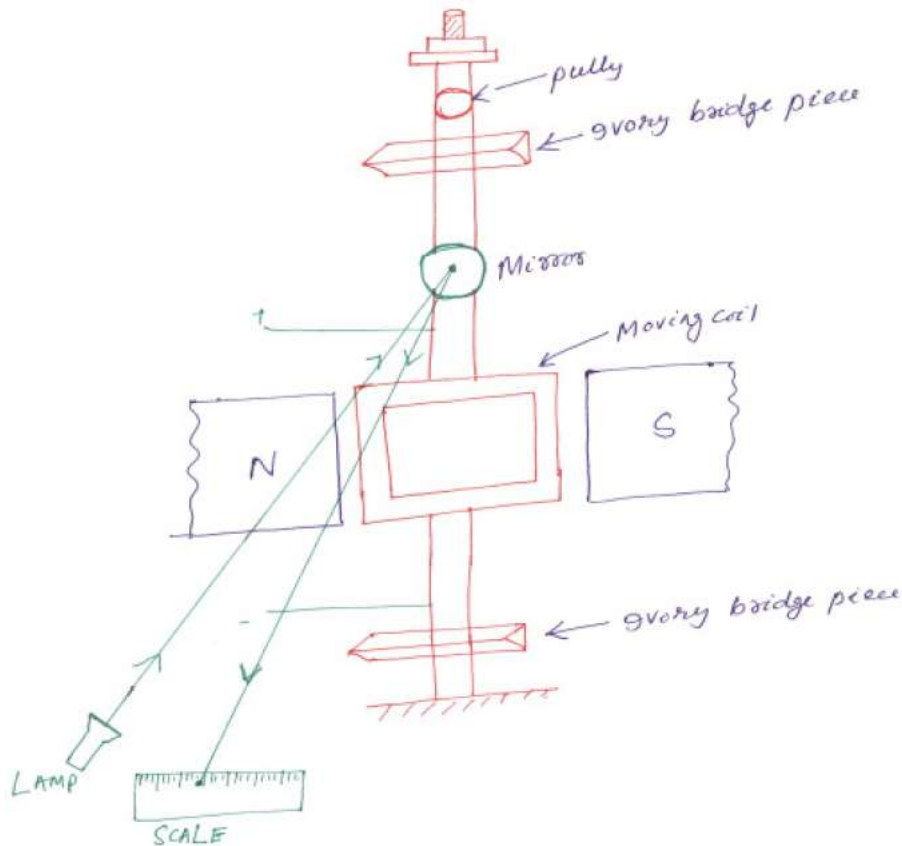


Fig 2.31 Vibration Galvanometer

**Example 2.2-**In a low- Voltage Schering bridge designed for the measurement of permittivity, the branch 'ab' consists of two electrodes between which the specimen under test may be inserted, arm 'bc' is a non-reactive resistor  $R_3$  in parallel with a standard capacitor  $C_3$ , arm CD is a non-reactive resistor  $R_4$  in parallel with a standard capacitor  $C_4$ , arm 'da' is a standard air capacitor of capacitance  $C_2$ . Without the specimen between the electrode, balance is obtained with following values ,  $C_3=C_4=120 \text{ pF}$ ,  $C_2=150 \text{ pF}$ ,  $R_3=R_4=5000\Omega$ .With the specimen inserted, these values become  $C_3=200 \text{ pF}$ ,  $C_4=1000 \text{ pF}$ ,  $C_2=900 \text{ pF}$  and  $R_3=R_4=5000\Omega$ . In such test  $w=5000 \text{ rad/sec}$ . Find the relative permittivity of the specimen?

**Sol:** Relative permittivity( $\epsilon_r$ ) =  $\frac{\text{capacitance measured with given medium}}{\text{capacitance measured with air medium}}$

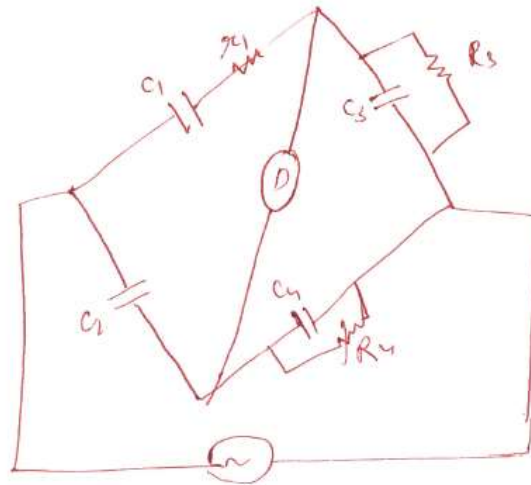


Fig 2.32 Schering bridge

$$C_1 = C_2 \left( \frac{R_4}{R_3} \right)$$

Let capacitance value  $C_0$ , when without specimen dielectric.

Let the capacitance value  $C_S$  when with the specimen dielectric.

$$C_0 = C_2 \left( \frac{R_4}{R_3} \right) = 150 \times \frac{5000}{5000} = 150 \text{ pF}$$

$$C_S = C_2 \left( \frac{R_4}{R_3} \right) = 900 \times \frac{5000}{5000} = 900 \text{ pF}$$

$$\epsilon_r = \frac{C_S}{C_0} = \frac{900}{150} = 6$$